

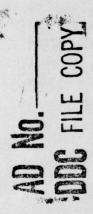
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Users Guide for ESD LORAN Grid Prediction Program

SAMUEL HOROWITZ





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The purpose of the LORAN Grid Prediction Computer program is to transform geographic coordinates into a LORAN time difference (TD). Utilizing

available map data of terrain and lithology and applying an integral form of Maxwells' equations, the propagation time of a low frequency pulse over irregular and inhomogeneous ground can be calculated. The method of data tape production and TD calculation is described with program listings. The technique has been successfully used by several U.S. Government agencies.

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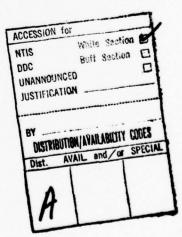
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Preface

This work was performed at the request of the LORAN Systems Project Office, Electronic Systems Division, Hanscom AFB, MA 01731.

The type of program described in this paper involved numerous people for its success, in particular: Dr. Terence J. Elkins, RADC/EEP, Capt. Randolf Gressing, ESD/DCL, and Mr. William McComish, Boston College. Deeply appreciated are their vigorous and indispensable technical support.



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Users Guide for ESD **LORAN** Grid Prediction Program

1. INTRODUCTION

The ability to precisely deliver ordnance or men and material under all weather conditions in an adverse battlefield environment, is one of the most severe requirements imposed on U.S. Worldwide Tactical Air Forces. A key element in meeting this requirement involves obtaining and providing position data in a specified coordinate system, to allow navigation of tactical aircraft to desired locations with sufficient accuracy for rendezvous or weapon release. The LORAN radio navigation system is being relied upon more and more as a principle source of navigation information in tactical airborne operations. Position indication is given in terms of LORAN TD's (time difference) which, because of propagation anomalies, do not correspond precisely to earth fixed geodetic coordinates. Therefore, each LORAN chain requires a grid prediction for its coverage area. Such a grid prediction computer program package has been developed at RADC/ EEP and is described herewith. This manual contains sufficient information to enable the experienced programmer to understand the programming aspects of LORAN grid prediction and includes a detailed functional description and its operation.

2. SYSTEM CONFIGURATION

The operation of the entire LORAN Grid Prediction System from obtaining the required input data off maps to the calculation of the output time difference is illustrated in Figure 1. The system has been divided into the four following parts:

PART I: Formation of map digitized.

PART II: Calculation of surface impedance data base.

PART III: Field LORAN prediction package.

PART IV: Updating data base by comparison of calculated and experimental results.

A sufficient description of the various computer program is presented so that the user can obtain the required LORAN coordinates. The data base is generated in PARTS I and II and updated when measured data is available in PART IV. In PART III of the systems, the main set of calculations are performed and this is described first in Section 3. The technique for translating the earth's electrical properties into a surface impedance and properly sequenced onto a rapid access magnetic disc is described in Section 4. Brief description of map data digitization and system tuning or data base updating is given in Sections 5 and 6, respectively.

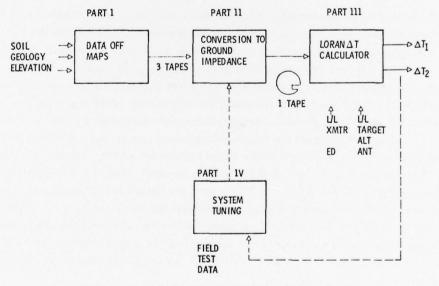


Figure 1. Total LORAN Grid Prediction System

3. DESCRIPTION OF PART III

3.1 Overview

A block diagram of the PART III LORAN prediction package is shown in Figure 2. Its purpose is to furnish the LORAN TD's for a desired target given the ground properties of the system coverage area. For each LORAN chain, the geodetic location of the master and two slave transmitters must be known in addition to the two slave emission delays. A magnetic tape of the ground electrical properties for the given coverage area is also required. The latitude and longitude of the desired target and delivery altitude are inserted into the program and a time of arrival (TOA) from each of the transmitters is computed. Subtracting the master TOA from each of the slave TOA's yields two TD's which determine the LORAN coordinates of the target.

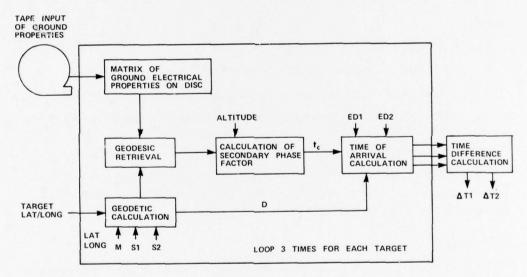


Figure 2. LORAN Prediction Package - Part III

The operation of this program can be followed by referring to Figure 2. The input tape contains the ground electrical properties which consist of elevation and complex surface impedance for the area of interest. This is in the form of a matrix of data points every 30 arc sec in latitude and longitude. The information is recorded onto a disc for rapid access of data between any two points in the service area as required by the geodesic retrieval.

The input data cards contain the following: (a) transmitter coordinates with associated emission delays, and (b) target coordinates, delivery altitude, integration step size, and type of receiving antenna for each target. This data is first used in the geodetic calculation to determine path length (D) between each of the transmitters and the target, and to determine points along the geodesic path governed by the distance increment or integration step size. The points along the geodetic path are input to the geodesic retrieval, which in turn obtains the ground electrical properties of the points from the matrix on the disc. This information is used to calculate the time correction or secondary phase factor due to the decrease in propagation velocity, compared to free space, when a signal propagates over the earth's surface. Time of arrival calculations can then be made from the following equation:

$$TOA = \frac{n}{c}D + t_{c} + ED \tag{1}$$

where

n = atmospheric index of refraction = 1.000338.

c = velocity of light = 2.997925 × 10⁸ meters/second.

D = length of geodetic path from transmitter to receiver in meters.

 $t_{\rm c}$ = time correction or secondary phase factor for propagation over a given path length in $\mu {\rm sec.}$

ED = emission delay in μ sec.

Three such calculations, one from each transmitter to target, are required for each prediction. Subtracting the master TOA from each of the slave TOA's, one obtains the LORAN coordinate prediction.

3.2 Prediction Program Flow Chart

A flow chart illustrating the operation of the LORAN Grid Prediction package is illustrated in Figure 3 and subroutine relationships to the driving program LORANCO is shown in Figure 4. This package consists of a deck with approximately 1300 cards and requires a core memory of 120K base eight (8). The three transmitter (M, S1, S2) coordinates with corresponding emission delays are read into the program from the input data deck. For computation purposes, the geographic coordinates are converted into radians by a call to subroutine CORRAD. The target coordinates are then read into the program with corresponding information on delivery altitude in meters, computation step size in kilometers, and type of receiving antenna (Electric dipole = 1, Loop = 0). Similarly, these coordinates are converted to radians. The program is terminated when the step size (ADELS)

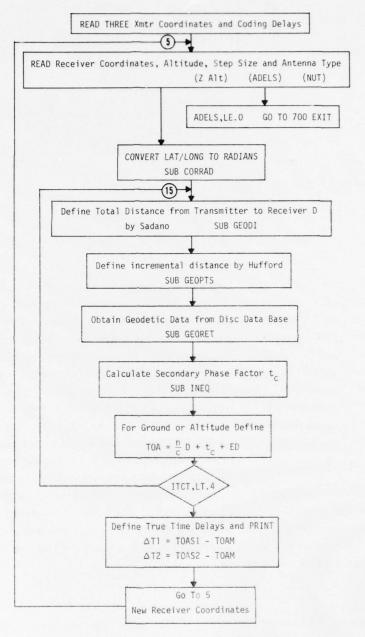


Figure 3. LORAN Program Flow Chart

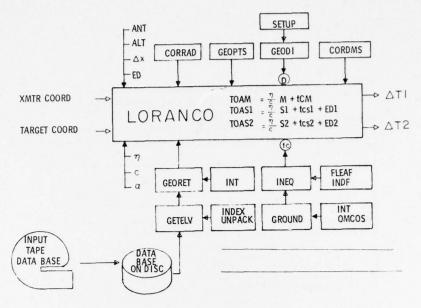


Figure 4. ESD LORAN Grid Prediction Program

is equal to or less than zero. Therefore, a blank card after the last desired target card causes the program to exit. With information on transmitter and target location, the program can now determine the propagation path. The total geodesic distance for primary wave delay is calculated in subroutine GEODI which uses the Sodano formulation. 1, 2 The coordinates of incremental points along the propagation path are defined in subroutine GEOPTS. The ground electrical properties for these points are obtained through subroutine GEORET which in turn calls subroutine GETFLV. In the latter subroutine, the required points are indexed to address data for the random access disc. Upon return from the disc, the data is unpacked and returned to GEORET. With a detailed description of the points along the propagation paths available, one can now calculate the secondary phase factor or time correction, tc, due to the disturbing influence of the earth using the Hufford Integral formulation equation. 3, 4, 5 Ninety-five percent of the compute time is required for this calculation in subroutine INEQ. The time of arrival is the sum of the primary wave travel time, secondary phase factor, and emission delay. All the required information for this calculation over a given path is now available and the resultant calculation is stored.

Due to the large number of references on this page, the references will not be footnoted. See references, page 83.

The above procedure is repeated three times, once from each transmitter to receiver by looping back to statement 15 after each completed TOA. With the completion of the TOA calculations, the predicted time difference for a given geographical coordinate is calculated (T, T2) in the driving program LORANCO and output printed. Control is then transferred back to statement 5 where new target coordinates are read into the system, and the entire process is repeated until ADELS is made equal to or less than zero.

Figure 4 is an additional flow chart illustrating the subroutine relationships to the driving program LORANCO.

3.3 Data Input and Output Setup

3.3.1 INPUT

Program LORANCO requires a data deck and data tape for operation loaded as shown in Figure 5. The data deck supplies the geographic location of transmitters and targets and additional required constants such as emission delay, altitude, step size, and type of receiver antenna. The data tape supplies the ground electrical properties for the entire service area covered by the transmitters.

The first three cards in the data deck describe the transmitter input data as follows:

Cols	Data	Format
1-2	Blank	
3-6	Alpheric numeric identifier for transmitter	3A8
26-42	Latitude data	I5, I3, F7.3, A1
26-30	Latitude, degrees	I5
31-33	Latitude, minutes	13
34-41	Latitude, seconds	F7.3
42	Latitude, N or S	Al
43-58	Longitude, data	I5, I3, F7.3, A1
43-47	Longitude, degree	I5
48-50	Longitude, minutes	I 3
51-57	Longitude, second	F7.3
58	Longitude, E or W	A1
59-78	Emission Delay	F20.3

All degrees, minutes, and seconds are right justified in their respective field. Emission delay is in units of μ sec. The order of transmitter cards are master, slave 1, and slave 2. The master emission delay will always be zero. Slave 1 emission delay is always less than that of slave 2.

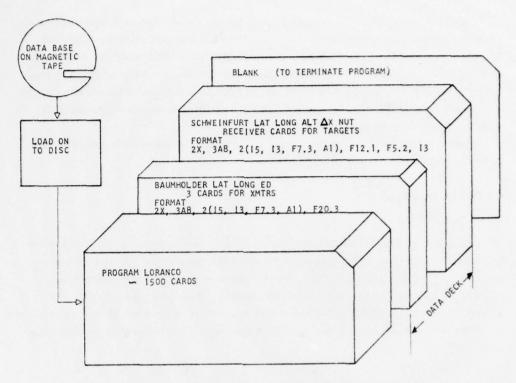


Figure 5. Deck Setup for Program LORANCO

The next set of cards contain the target input data. It is read in as one target per card so there will be as many receiver cards as targets with the following format:

Cols	Data	Format
1-2	Blank	
3-26	Alpheric numeric identification for receiver identification	3A8
26-42	Latitude data	I5, I3, F7.3, A1
26-30	Latitude, degrees	15
31-33	Latitude, minutes	I3
34-41	Latitude, seconds	F7.3
42	Latitude, N or S	A1
43-58	Longitude data	I5, I3, F7.3, A1
43-47	Longitude, degrees	I5
48-50	Longitude, minutes	I3

Cols	Data	Format
51-57	Longitude, seconds	F7.3
58	Longitude, E or W	A1
59-70	Altitude, meters	F12.1
71-75	Step Size, kM	F5.2
76-78	Type of Antenna	13

The aircraft altitude at the release point is specified in meters and the distance increment or step size in kilometers typically 0.5 kilometers. NUT defines the type of receiver antenna. For a vertical antenna, a 1 is placed in column 78, for a loop, a 0 in column 78. A blank card or zero in columns 71-75 will terminate the program.

The data tape contains information on the electrical properties of the ground and covers the entire service area. Points selected outside this area will cause the program to print "OUT OF ACCEPTABLE RANGE, FURTHER CALCULATIONS FOR THIS PATH HAVE BEEN DELETED." The supplied magnetic tape contains 5760 records of 60 words each with each word representing 120 data points or one degree of latitude. Each data point is defined by a complex surface impedance and an elevation. The current area covered is 66 to 14 degrees in longitude and 48 to 54 degrees in latitude. This tape is read into the random access data base disc unchanged in format with the sequential record number on the tape becoming the random access index array address number. No operation on the tape is required.

3.3.2 OUTPUT

Program LORANCO produces the following printed output:

- (a) For each transmitter, an echo printout of columns 3-58, of the input card.
- (b) For each receiver, an echo printout of columns 3-58 of the input card.
- (c) For each transmitter to receiver path, geodesic path information, and a printout of the parameters used by subroutine INEQ.
- (d) Results of the ground wave time delay calculations in the form of the list NAMI. The list NAMI contains information on time of arrivals (TOA), time delays (TD1, TD2), emission delays (ED1, ED2), geodesic distances (DISTSOD), primary wave times (TPW), and secondary phase factor times (TIMDUM).

3.4 Program Subroutines and Functions

LORANCO - Reads inputs, defines three paths, calls data base and INEQ, calculates TOA and TD.

CORRAD - Degrees (Lat, Long) to radians.

CORDMS - Radians to degrees (Lat, Long).

GEOPTS - Defines points along geodetic from transmitter to receiver.

INT - Calculate first and second derivative of elevation.

GETELV - Read geophysical data off disc.

UNPACK - Unpack data from disc.

GEORET - Returns geophysical data to driving program.

INEQ - Solution of integral equation for secondary phase factor.

INDF - Induction field calculation (E or H field).

CNEUKEN - Interpolation routine for integration.

GEODI - Calculation of total geodetic distance by Sodano and back azimuth.

SETUP - Constants for spheroid to be used.

GROUND - Introduces variable ground impedance and variable ground terrain into integral equation formulation of the ground wave.

CANG - Calculates argument of a complex number.

INDEX - Calculates index values of data base variables from LAT/LONG.

WERF - Calculates error function.

OMCOS - Calculates 1 - cos (X).

FLEAF - Calculates ground wave attenuation function over flat ground using flat earth theory.

3.5 Subroutine Description

3.5.1 LORANCO

This is the driving module for the entire program. It reads the input coordinates of both transmitters and receivers, defines the geodesic path, receives data base parameters and calculates the secondary phase factors, time of arrivals, and time difference. The first three read cards, one for each station, furnish the transmitter locations and associated emission delays. A call to CORRAD changes the units of the input data from degrees to radians. The first target or receiver geographic coordinates are then read in degrees, and changed to radians by a call to CORRAD. The various paths from transmitter to target and then defined (RLA(ITCT), RLO(ITCT)), and a call to subroutine GEOPTS defines the incremental path coordinates. The call to subroutine GEODI returns the total distance from transmitter to target (SBKMS) by a Sodano calculation. ² This value is later used to calculate the primary wave delay. With the incremental geographic coordinates known along the geodesic, the call to subroutine GEORET returns the ground electrical properties of elevation and impedance through common blocks/GROUND/and/ SDRDI/for use in subroutine INEQ. Subroutine INEQ determines the secondary phase factor, TIMSAV. The time of arrival (TOA) for a given path (ITCT) is determined from the relationship:

TOA (ITCT) = ENC * SBKMS + TIMSAV

(2)

where ENC = ground refractive index divided by the velocity of light. ITCT is then incremented for a new path between the next transmitter in the chain and the same receiver, and program control returns to statement 15 where RLA(ITCT) and RLO(ITCT) are redefined. The above process is then repeated until three TOA'S are calculated. The required time difference (TDI) then computed from the relation:

$$TDI = EDI + TOA(2) - TOA(1)$$
(3)

where

EDI = emission delay for slave 1.

TOA(2) = Time of arrival for slave 1 at receiver, TOAS1.

TOA(1) = Time of arrival for Master at receiver, TOAM.

When the calculations are performed for airborne locations, the secondary phase factor contains an altitude correction derived in subroutine INEQ and defined as ALTTMSV.

Upon completion of the time difference calculation, control is transferred back to statement 5 in the program where the information for the next target is read in and the entire process repeated. The program exits when the step size (ADELS) on the target card is equal to or less than zero.

3.5.2 SUBROUTINE CORRAD

Subroutine CORRAD transforms degrees into radians for a given latitude or longitude. The subroutine statement is SUBROUTINE CORRAD (RCOR, IDEG, IMIN, SEC, ID, IS, IERR) where:

RCOR = Location in radians.

IDEG = Location in degrees.

IMIN = Location in minutes.

SEC = Location in seconds.

ID = Character for north, south, east, or west.

IS = Latitude or longitude indicator.

IERR = Error code.

This subroutine is called from the driving program and returns radians to the driving program through the argument list. It is used to transform the input transmitter and receiver coordinates into radians.

3.5.3 SUBROUTINE GEOPTS

Given the distance S_p from point A to a point P on the geodesic between two prescribed points A, B, on the surface of a spheroidal earth, the FORTRAN subroutines GEOPTS returns the latitude \emptyset_p , and longitude θ_p of P, and the forward azimuth ψ_p of the geodesic of P as shown in Figure 6.

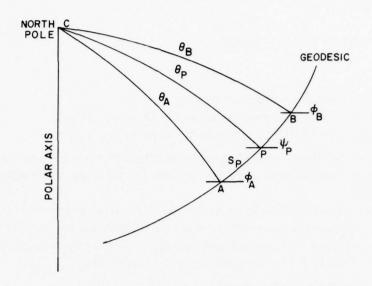


Figure 6. Geodesic Geometry

The derivation of the equations under the subroutine are described by Spies. 6 The subroutine statement is: SUBROUTINE GEOPTS (SMP, RLATP, RLONP, RAZP) where

 $SMP = S_p = distance (in meters) of P from A,$

RLATP = \emptyset_{D} = latitude (in radians) of P,

RLONP - $\theta_{\rm p}$ = longitude (in radians) of P,

and

RAZP = ψ_{p} = forward azimuth (in radians) of geodesic of P.

Latitudes θ_A , θ_B and longitudes θ_A , θ_B of the prescribed end-points A, B are stored in the COMMON block PATH, along with certain output parameters. We

Spies, K.P. (1975) The Analytical Basis of Hufford's Computer Technique for Determining Topographic Profiles, Institute for Telecommunication Services Memo dated Nov. 4, 1975.

have the statement: COMMON/PATH/PLATA, RLONA, RIATB, RLONB, RAZA, RAZB, SMB, where

RLATA = \emptyset_A = latitude (in radians) of A,

RLONA = θ_A = longitude (in radians) of A,

RLATB = $\emptyset_{\mathbf{R}}$ = latitude (in radians) of B,

RLONB = θ_{R} = longitude (in radians) of B,

RAZA = ψ_A = forward azimuth (in radians) of geodesic of A,

RAZB = ψ_{B} = forward azimuth (in radians) of geodesic of B,

and

SMB = S_B = length (in meters) of geodesic from A to B.

North latitudes and east longitudes are positive, whereas south latitudes and west longitudes are negative. Positive azimuths are measured clockwise from north.

Parameters which specify relevant dimensions of the spheroidal earth are defined in the DATA statement: DATA ASPH, ESQ, CESQ/6378206.4, 0.006768658, 0.993231342/ where

ASPH = a = length (in meters) of semimajor axis of spheroid,

 $ESQ = e^2 = (a^2 - b^2)/a^2$ (where b is length of semiminor axis of spheroid),

 $CESQ = 1 - e^2$.

and the numerical values correspond to the Clarke spheroid of 1866. Any other desired spheroid can be used in GEOPTS simply by replacing the above DATA statement by one containing the appropriate numerical values. For example, for the International spheroid, one would use:

DATA ASPH, ESQ, CESQ/6378388.0, 0.006722670, 0.993277330/.

As we shall see in the following section, the quantities \emptyset_p , θ_p , ψ_p , are approximated by esculatory cubic polynomial functions of the distance S_p of P from A; for a fixed spheroid, the coefficients in these polynomials depend only on the location of the end-points A, B. To achieve computational efficiency in situations where \emptyset_p , θ_p , ψ_p are to be calculated for more than one point P on the geodesic between a fixed pair of end points, GEOPTS is provided with a second entry point PCOORD (by including the ENTRY statement ENTRY PCOORD), whereby the subroutine skips the coefficient calculations and proceeds directly to the evaluation of the polynomial expressions for \emptyset_p , θ_p , ψ_p . For a given pair of end-points A and B, the initial call to the subroutine must use the main entry point GEOPTS: that is, the calling program reference must be

CALL GEOPTS (etc., etc., ...).

Since the polynomial coefficients have already been evaluated, subsequent calls (for that path) should then use the entry point PCOORD: that is, the calling program reference should be:

CALL PCOORD (etc., etc., ...).

It is thus evident the subroutine GEOPTS is particularly efficient in those cases where \emptyset_{D} , θ_{D} , ψ_{D} are desired for several to many points P on a single geodesic.

3.5.4 SUBROUTINE GEORET

This subroutine is called from the driving program LORANCO. Subroutine GEORET obtains from the data through GETELV the values of elevation and impedance which occur at intervals along a geodesic specified by arrays LAT and LON. The path elevation and impedance data are transmitted to the driving program via blocked common statements.

The subroutine statement is SUBROUTINE GEORET (LAT, LONG, DSKM, NP) where:

LAT = Array of latitudes along a geodesic path.

LON = Array of longitudes along a geodesic path.

DSKM = Distance along geodesic path in KM.

NP = Number of points along the geodesic path.

To obtain elevations and impedances from the data base, GEORET steps through NP latitude and longitude points calling GETELV each time. Amplitude and phase data are returned, converted to real and imaginary values, and stored in arrays DR and DI. Elevation information is stored in array Z. Subroutine GEORET then calls subroutine INT to obtain the first and second derivative of the elevation data.

Support information required by GEORET and supplied by common blocks include:

- (1) Common/GROUND/
- (2) Common/INDUCT/
- (3) Common/TE/
- (4) Common/SDRDI/
- (5) Common/CITCT/

By use of common blocks, certain of the information can be directed to the double integral subroutine (INEQ) and its support subroutines, while other control data are transmitted to the driving section of the overall program.

3.5.5 SUBROUTINE GETELV

This subroutine is called from subroutine GEORET. Subroutine GETELV indexes the input latitude and longitude coordinates for subroutine UNPACK to obtain the proper ground electrical properties off the disc.

The subroutine statement is SUBROUTINE GETELV (LAT, LONG, AMP, FAZ, ELVTN) where:

- LAT, LON The input coordinate of each incremented point along the geodesic path.
- AMP, FAZ, ELVTN = The output complex impedance (AMP, FAZ) and elevation (ELVTN) from the disc data base.

Two indices are selected of adjacent longitude records, NPACK, which encompass the input coordinate. These two records are separated by 30 in. in longitude and cover a latitude of one degree or 120 points. The elevation data, ELVTN, is obtained by a linear interpolation within the 30 in. square surrounding the desired coordinate, and is stored in eleven bits of the available thirty bit word. The impedance data of the southwest corner of the 30-in. square is used to represent the entire square. No impedance interpolation is required. For the complex impedance data, eight bits are used for the magnitude and eleven bits for the phase.

The impedance and elevation data are returned to subroutine GEORET through the argument list.

3.5.6 SUBROUTINE SETUP

This subroutine provides the spheroidal data for subroutine GEODI. Inputs are the semimajor (AO) and semiminor (BO) axis of the earth in meters. The spheroidal flattening (FL) and eccentricity square (ESQ) are calculated. The spheroidal constants for various ellipsoids are:

Ellipsoid	Semimajor	Semiminor	
International	6378388.0	6356911.9	
Clarke 1866	6378206.4	6356583.8	
Clarke 1880	6378249.1	6356514.9	
Bessel	6377397.2	6356079.0	

Subroutine SETUP is called from subroutine GEODI and returns the required constants through the COMMON/GENERAL/block.

3.5.7 SUBROUTINE INT

Subroutine INT is called by subroutine GEORET and calculates the first and second derivative of the elevation at each point along the geodesic path. The subroutine statement is SUBROUTINE INT (I.K) where:

I = Position in x and z arrays on which to center calculations.

K = Position in arrays Z and ZP to store calculated values.

An analytical expression for a parabolic fit to three data points closest and including the required point along the geodesic path is derived by Sheed. Differentiating this curve twice yields the required first and second derivative of the elevation at the position on which the calculations are centered. The results are returned to GEORET for use in subroutine INEQ via Common/Ground/block.

3.5.8 SUBROUTINE UNPACK

Subroutine UNPACK takes each sixty word record from the data base and unpacks each word into two complete data points composed of elevation and impedance information. Each called record contains the data for 120 points. The original sixty-bit words when unpacked, allow thirty bits for each data point. These are allocated as follows:

Elevation in meters, ELEV, 11 bits, ±7 meters.

Magnitude of Impedance, AMP, 8 bits, ±2 ohms.

Phase of Impedance, FAZ, 11 bits, ±0.001 radians.

The information obtained is returned to GETELV.

For machines with 32 bit words, the UNPACK subroutine is altered so that one data point is obtained from each word.

3.5.9 SUBROUTINE INEQ

Subroutine INEQ is called from the driving program, LORANCO, and returns the secondary phase factor or additional time correction. The LAT and LON in the calling statement are the array of path length latitudes, and longitudes respectively.

The following constants are first set for the operation of this program:

NUT = 0 or 1 depending on type of receiver antenna.

RAD = radius of earth = 6.36739×10^6 meters.

ALPHA = Vertical lapse factor = 0.85.

FREQ = Frequency = 0.1 MHz.

NSTART = Index of first distance at which the field is to be found as a function of altitude = 0.5 km.

ETA = Refractive index = 1.000338.

^{7.} Sheed, F. (1962) Theory and Problems of Numerical Analysis, Shaum's Outline Series, McGraw Hill Co.

The attenuation function is calculated at discrete points as a function of geodesic distance. ⁸ The amplitude or modulus of the complex attenuation function is the field intensity and the phase or argument is the secondary phase correction in radians. To solve for this attenuation function, the boundary conditions must be known, then the solution can be extended step by step by numerical integration.

By assuming that the ground is smooth just in front of the transmitter, the first few points can be calculated with classical formulas. ⁹ For the remaining points, an integral equation approach is employed which allows one to introduce variations in ground elevation and variations in ground impedance relative to a classical spheroid. Special care must be exercised in the integration near the beginning and end of the integration path because the integrand approaches infinity at these points. A Gaussian quadrature integration formula ¹⁰ is employed in the area of such singularities, and Simpson's rule is used in the rest of the interval. The effective ground impedance which combines the elevation and impedance variations is obtained through a common statement from subroutine GROUND. After the calculations along the ground are completed for a given transmitter to receive path, a height gain loop ^{4, 11} is activated if the altitude input data is other than zero. Upon completion of the integration, the results are returned to the driving program through common block/DELAY/.

Input information initially obtained by the driving program from the stored disc data base is transmitted to subroutine INEQ via common blocks:

Common/GROUND/and Common/TE/

Transmitter-receiver path increment data enters via common blocks:

Common/SS/and Common/SDRDI/

Integral equation control of variables from the driving program into subroutine INEQ enter via:

Common/CITCT/

Calculations of secondary phase factors in units of microseconds are returned to the calling program via:

Common/DELAY/

^{8.} Johler, J.R., and Horowitz, S. (1973) Propagation of LORAN-C Ground and Ionospheric Wave Pulses, Office of Telecommunications Report 73-20 (Superintendent of Documents, U.S. Government Printing Office, Washington, D.C. 20402).

Johler, J.R., Keller, W.J., and Walters, L.C. (1956) Phase of the Low Radiofrequency Ground Wave, NBS Circular 573 (Superintendent of Documents, U.S. Government Printing Office, Washington, D.C. 20402

Abramovitz, M. and Stegun, I. (1964) <u>Handbook of Mathematical Functions</u> – NBS - Applied Math Series 55, U.S. Government Printing Office.

^{11.} Scott, R. (1966) Phase of the Height-Gain Function of the Low Frequency Ground Wave, Report 2900-156-T of Project Michigan (Willow Run Laboratories, Ann Arbor, Michigan 48106).

```
PROGRAM LCRANCO(INPUT=128, CUTPUT=128, TAPE2)
    DIMENSION IDENTF (3)
    DIMENSTON LAT (999) , LON (999)
    DIMENSION DISTRUM(3), TIMDUM(3)
    DIMENSION TOA(3)
    DIMENSION DISTSOD(3)
    DIMENSION TPW(3)
    DIMENSION ALTTHSV(3,2)
    DIMENSION FATHL (3)
    DIMENSION LOUM(3,4), ADUM(3,4), RLA(3), RLO(3)
    COMMON/PATH/RLATA, RLONA, PLATB, RLONB, RAZA, RAZB, SBM
    COMMON/CITCT/ITCT, LTOP, ALTT MSV
    COMMON/DEL AY/NP, DISTSAV, TIMSAV
    COMMON/ZOTA/ARRAY(40)
    NAMELIST/NAM1/TOA, TD1, TD2, ED1, ED2, DISTOUM, TIMOUM, DISTSCO
   1,TPW
    DATA
          RTODEG/57.2957795130823/
    DATA ITCT/1/
    DATA ARRAY/100.,1.000338,46.,.1,5.,1.,3.,3600.,10.,0.,1000.,
          .85,0.,1.,26*0./
    C=.299792
    EN=1.000338
    ENC=EN/C
     READ TRANSMITTER COORDINATES FOR MASTER, S1, S2.
    PRINT 101
    PRINT 13
101 FORMAT (*1TRANSMITTER COORDINATES*)
    MISKOD=0
    DO 913 I=1,3
    READ 102, ICENTF, LDUM(I,1), LCUM(I,2), ADUM(I,1), ADUM(I,2),
              LOUM (I, 3), LOUM (I, 4), ADUM (I, 3), ADUM (I, 4), TOA (I)
    PRINT 163, IDENTF, LDUM(I,1), LDUM(I,2), ADUM(I,1), ADUM(I,2),
               LDUM(I,3),LDUM(I,4),ADUM(I,3),ADUM(I,4)
   1
102 FORMAT(2X,3A8,2(15,13,F7.3,A1),F12.1,F5.2,13)
103 FORMAT(2x, 3A8, 2(2x, 15, 13, F7.3, A1))
104 FORMAT (*1RECEIVER COORDINATES*)
    CALL CCPRAC(RLO(I),LDUM(I,3),LDUM(I,4),ADUM(I,3),ADUM(I,4),1,MISKO
   10)
    CALL CCRRAD(RLA(I), LDUM(I,1), LDUM(I,2), ADUM(I,1), ADUM(I,2), 0, MISKO
    1F (MISKOD. EQ. 0) GO TO 913
    PRINT 23
    GO TO 10
913 CONTINUE
    E01=TOA(2)
    EDZ=TCA(3)
  5 CONTINUE
    PEAD 192, ICENTF, LATDEGR, LATMINB, SECLATB, LATIDB, LONDEGE, LONMINB,
   ISECLONE, LONIDB, ALT, ADELS, NUT
    IF (ADELS . LE.L) GO TO 10
    P? INT 104
    PRINT 13
    PRINT 103, IDENTF, LATOEGB, LATMINB, SECLATB, LATIDB, LONDEGE, LONMINE,
   1SECLONB, LCNIDB
    ARRAY (10) = ALT
    ARPAY (14)=NUT
    MISKOD=0
```

```
CALL CORRAD(RLATB, LATDEGB, LATMINB, SECLATB, LATIDB, 0, MISKOD)
    CALL CORRAD(RLONB, LONDEGB, LONHINB, SECLONB, LONIDB, 1, MISKOD)
    IF (MISKOD.EQ. 0) GO TO 15
 20 PRINT 23
 23 FORMAT(//11%, 3H***, 9%, 29HERROR IN END-POINT COORDINATE, 10%, 3H
   +***/11X,54H*** CALCULATIONS FOR THIS PATH HAVE BEEN DELETED ***)
    60 TO 5
 15 CONTINUE
    RLATA=RLA(ITCT)
    RLONA=RLO(ITCT)
 13 FORMAT (12H0 LOCATION, 22X, 8HLATITUDE, 9X, 9HLONGITUDE/
   1 26x,2(5x,13H(DEG-MIN-SEC))/)
    1 TOP=D
 25 CALL GEOPTS(0.0, RLATP, RLONP, RAZP)
    CALL GEODI (RLATA, RLONA, RAZAS, SBMS, RLATB, RLONB, RAZBS)
    SBKMS=SBMS*.001
    DAZA = RTODEG*RAZA
    DAZB = RTODEG*RAZB
    SBKH = SBH#1.0E-3
    DEL=SBKM-SBKMS
    PRINT 2, ITCT, SBKMS, SBKM, DEL
  2 FORMAT (*OGEODESIC DISTANCES, TRANSMITTER*12* (POINT A) TO RECEIVER
   1 (POINT 8) */7x*SODANO*9x*HUFFORD*6x*DIFFERENCE*/3F15.5)
    NP = SBKM/ADELS+1.0
    DSKM = NP
    DSM = SBM/DSKM
    DSKM = DSM#1.0E-3
    PRINT 33, SEKH, DSKH, DAZA, DAZB
 33 FORMAT(//18X, 20HLENGTH OF GEODESIC =, F11.5, 11H KILOMETERS//18X,
   + 28 HDIST ANCE INCREMENT =, F11.5, 11H KILOMETERS///12X, 34HFORWARD
   +AZIMUTH OF GEODESIC AT A =, F12.6, 8H DEGREES//12X, 34HFORWARD AZI +MUTH OF GEODESIC AT B =, F12.6, 8H DEGREES)
    LAT (1) = L DUM(ITCT, 1) + 10000 + LDUM(ITCT, 2) +100+ IFIX(ADUM(ITCT, 1))
    LON(1)=LOUM(ITCT,3) *10000+LOUM(ITCT,4) *100+IFIX(ADUM(ITCT,3))
    NPP2=NP+2
    SPH = 0.0
    DO 100 IP=1,NPP2
    SPH = SPH+DSM
    CALL PCOORD(SPM, RLATP, RLONP, RAZP)
    MISKOD = 0
    CALL CORDMS(RLATP, LATDEGP, LATMINP, SECLATP, LATIDP, 0, MISKOD)
    CALL CORDMS(RLONP, LONDEGP, LONMINP, SECLONP, LONIDP, 1, MISKOD)
    IF (MISKOD) 30,35,30
 30 PRINT 43, IP
 43 FORMAT(//2x, 62H*** ERROR DETECTED DURING CONVERSION OF COORDINAT +ES FOR POINT, 15, 5H ***/2x, 2H**, 7x, 52HFROM RADIANS TO (ALPHAM +ERIC) DEGREES-MINUTES-SECONDS, 7x, 3H***/2x, 3H***, 66x, 3H***/2x,
   + 3H***, 7%, 52HFURTHER CALCULATIONS FOR THIS PATH HAVE BEEN DELETE
+D, 7%, 3H***)
GO TO 5
 35 CONTINUE
    LAT (IP+1 )=LATDEGP*10000+LATMINP*100+IFIX (SECLATP)
    LON(IP+1 )=LONDEGP#10000+LONMINP#100+IFIX(SECLONP)
108 CONTINUE
    IP=NP+3
    CALL GEORET (LAT, LON, DSKM, IP )
     ADJUST NO OF PTS TO MATCH INEQUE.
```

C

NP=NP+1 CALL INE GZE (LAT, LON) +TIMSAV TOA (ITCT)=ENC*SBKMS TPW(ITCT) = ENC+SBKMS DISTSOD(ITCT) = SBKMS PATHL (ITCT)=SBKMS DISTDUM(ITCT)=DISTSAV TIMDUM(ITCT)=TIMSAV ITCT=ITCT+1 IF (ITCT.LT.4) GO TO 15 SIF (LTOP.LT.1) PRINT 410 410 FORMAT (*0 GROUNDWAVE TIME DELAY CALCULATION*) TD1=ED1+TOA(2)-TOA(1) TD2=ED2+TOA(3)-TOA(1) PRINT NAM1 IF (LTOP.LT.1) GO TO 6 DO 8 L=1,LTOP PRINT 7 7 FORMAT (*0 ALTITUDE TIME DELAY CALCULATIONS*) DO 9 I=1,3 TOA(I)=ENC*PATHL(I)+ALTTMSV(I,L) 9 CONTINUE TD1=ED1+TOA(2)-TOA(1) TD2=ED2+TOA(3)-TOA(1) PRINT NAM1 8 CONTINUE 6 CONTINUE ITCT=1 GO TO 5 10 CONTINUE PRINT 11 11 FORMAT (*G END OF INPUT DATA.*) END

SUBROUTINE GEORET (LAT, LON, DSKM, NP) DIMENSION LAT (999) , LON (999) COMMON /GROUND/ZDUM, Z, ZPDUM, ZP, XDUM, X, RO, DEN, R, U, OMX, MA 1 VE, R2, ZPP, D, DOD1, DDD2 COMMON/INDUCT/HAV COMMON/TE/TLA, TLON, RLAT, RLON, HLAT, HLON, ZPP1, DINC1, TPI, NPTS 1, ZMAZ, WTH COMMON /SDRDI/S(999), DR(999), DI(999), LLM DIMENSION ZDUM(6), Z(1009), ZPDUM(6), ZP(1009), XDUM(6), X(1009), 1 ZPP1 (1009) COMMON/CITCT/ ITCT COMPLEX D, DEN, DDD1, DDD2 TPI=6.283185307 TLA=LAT(1) TLON=LON(1) RLAT=LAT (NF) RLON=LON(NF) DINC1=DSKM NPTS=NP S(1)=0. X(1)=0. DO 1 I=1,NP AAMP=.0744\$FAZ=.74109\$Z(I)=2.

```
CALL GETELV(LAT(I),LON(I),AAMP,FAZ,Z(I))
      IF (I. GT. 1) S(I) = S(I-1) +DSKM
      DR(I) = AAMP * COS(FAZ)
      DI(I) = AAMP * SIN(FAZ)
    1 CONTINUE
      LLM=NP
C
       GENERATE INDEPENDENT PATH TERRAIN ELEVATIONS RELATIVE TO TRANSHIT
      Q=Z(1)
      Z(1)=0.
      DO 2 I=2,NP
      FOR NOW, CONVERT DISTANCE TO METERS. S(I)=S(I) #1000.
C
      X(I)=S(I)
      7(I) = 7(I) - Q
    2 CONTINUE
C
       OBRAIN ELEVATION DERAVITIVES.
      NPM1=NP-1
      DO 3 L=2, NPM1
      CALL INT (L,L)
      ZPP1(L)=ZPP
    3 CONTINUE
      ZP (1)=0.
      ZPP1 (1)=0.
      ZP(NP)=ZF(NP-1)
      ZPP1 (NF) = ZPP1 (NP-1)
      RETURN
      END
```

```
SUBROUTINE CORRAD(RCOR, IDEG, IMIN, SEC, ID, IS, IERR)
    DIMENSION IDS (4)
    DATA (IDS=1HN, 1HE, 1HS, 1HW)
   ISS = IS
    IF (ISS) 10,5,15
 5 IF (ID.EQ.IDS(1)) GO TO 25
IF (ID.EQ.IDS(3)) GO TO 30
10 IERR = 1
   RETURN
15 IF (ISS-1) 20,20,10
20 IF (ID.EQ.IDS(2)) GO TO 25
IF (ID.EQ.IDS(4)) GO TO 30
    IERR = 1
    RETURN
25 SIGN = 1.0
    60 TO 35
30 SIGN = -1.0
35 IF (IDEG-180) 40,40,10
40 IF (IMIN-60) 45,10,10
45 IF (SEC-60.0) 50,10,10
50 RCOR = SIGN*FLOAT(IDEG)*(1.74532925199433E-2)+FLOAT(IMIN)*
  + (2.90888208665722E-4)+SEC#4.84813681109536E-6
    RETURN
    END
```

```
SUBROUTINE GEOPTS(SMP, RLATP, RLOMP, RAZP)
   COMMON/PATH/RLATA, RLONA, RLATB, RLONB, RAZA, RAZB, SHB
   DATA ASPH, ESQ, CESQ/6378388.000, 6.722670022E-3, 9.932773300E-1/
   DATA PID2, PI, TWOPI/1.57079632679490, 3.14159265356979,
  + 6.28318530717959/
 IF (ABS(RLATA)-PID2) 5,10,10
5 IF (ABS(RLATB)-PID2) 15,10,10
10 PRINT 3, RLATA, RLATB
 3 FORMAT(1H1, 89H SUBROUTINE GEOPTS CALLED WITH END-1921...
+E OUT OF ACCEPTABLE RANGE (-PI/2, PI/2) //13X, 16HLATITUDE OF A =,
+FR.2. 29H RADIANS LATITUDE OF B =, F8.2, 8H RADIANS)
                       SUBROUTINE GEOPTS CALLED WITH END-POINT LATITUD
13 FORMAT (33X, 28HPROGRAM EXECUTION TERMINATED)
   STOP
15 IF (ABS(RLONA)-TWOPI) 20,20,25
20 IF (ABS(RLONB)-TWOPI) 30,30,25
25 PRINT 23, RLONA, RLONB
23 FORMAT (1H1, 88H SUBROUTINE GEOPTS CALLED WITH END-POINT LONGITU
  +DE OUT OF ACCEPTABLE RANGE (-2PI, 2PI)//10x, 17HLONGITUDE OF A =,
  +F9.2, 31H RADIANS
                             LONGITUDE OF B =, F9.2, SH RADIANS)
   PRINT 13
   STOP
30 ALONR = RLONA
   BLONR = RLONB
   IF (ALONR+PI) 35,35,40
35 ALONR = ALONR+THOPI
40 IF (BLONR+PI) 45,45,50
45 BLONR = BLONR+THOPI
50 BLON = BLONR-ALONR
   IF (BLON+PI) 55,70,75
55 IF (BLONR) 60,65,65
60 BLONR = BLONR+THOPI
   GO TO 95
65 ALONR = ALONR-THOPI
GO TO 95
78 PRINT 33
33 FORMAT (1H1, 88H
                        GEODESIC PATH INCLUDES A GEOGRAPHIC POLE - SUBR
  +OUTINE GEOPTS CANNOT HANDLE THIS CASE)
   PRINT 13
   STOP
75 IF (BLON-PI) 95,70,80
80 IF (BLONR-PI) 90,98,85
85 BLONR = BLCNR-TWOPI
   60 TO 95
90 ALONR = ALONR+THOPI
95 SMB = RLATA+RLATB
   HETA = SIN(0.5*SMB)
   HETA = (1.8-ESQ#HETA#HETA)/CESQ
   HLAT = ASPY/(HETA+SQRT (HETA+CESQ))
   BLON = BLONR-ALONR
   ALON = HETA*BLON
   Q = SIN(ALON)
   BLAT = COS (RLATB)
   ALAT = COS(RLATA)
   SAZA = Q+BLAT
   SAZB = Q*ALAT
   Q = SIN(0.5*ALON)
```

Q = Q*Q AAZ = RLATB-RLATA CA ZB = (1.0-Q) *SIN (AAZ) Q = Q*SIN(SMB) CAZA = CAZE+Q CAZB = CAZB-Q Q = SQRT (SAZA+SAZA+CAZA+CAZA) SMB = HLAT*ASIN(Q) SAZA = SAZA/Q CAZA = CAZA/Q SAZB = SAZE/Q CAZB = CAZB/Q RAZA = ATAN2(SAZA, CAZA) RAZB = ATAN2(SAZB, CAZB) ALON = RAZE-RAZA IF (ABS(ALCN)-PI) 120,105,105 105 IF (ALCN) 110,110,115 110 RAZB = RAZB+THOPI GO TO 120 115 RAZA = RAZA+TWOPI 120 H_AT = CESC+ESQ*ALAT*ALAT HLON = ASPH/SQRT (HLAT) HLAT = HLON=CESQ/HLAT HLON = HLON*ALAT CLAT = CAZA/HLAT CLON = SAZA/HLON HLAT = CESQ+ESQ+BLAT+BLAT HLON = ASPH/SQRT (HLAT) HLAT = HLON*CESQ/HLAT HLON = HLON*BLAT ALAT = CAZE/HLAT BLAT = (3.0+AAZ/SMB-ALAT-2.0+CLAT)/SMB ALON = SAZB/HLON BLON = (3.0*BLON/SHB-ALON-2.0*CLON)/SHB AAZ = 3.0*SMB ALAT = ((ALAT-CLAT)/SMB-2.0+BLAT)/AAZ ALON = ((ALON-CLON)/SMB-2.0*BLON)/AAZ AAZ = (RAZB-RAZA)/SMB ENTRY PCOORD RLATP = ((ALAT*SMP+BLAT)*SMP+CLAT)*SMP+RLATA RLONP = ((ALON*SMP+BLON)*SMP+CLON)*SMP+ALONR RAZP = AAZ*SMP+RAZA RETURN END

SUBROUTINE CORDMS(RCOR, IDEG, IMIN, BEC, ID, IS, IERR)
DIMENSION IDS(4)
DATA (IOS=11M, 1HE, 1HS, 1HW)
RANG = RCOR
SEC = ABS(RANG)*206264.806247096
ISS = IS
IF (ISS) 5,10,15
5 IERR = 1
RETURN
10 IF (SEC-324000.0005) 25,5,5
15 IF (ISS-1) 20,20,5
20 IF (SEC-648000.0005) 25,5,5

```
25 IF (RANG) 30,35,35
30 ISI = 2
   GO TO 40
35 ISI = 0
40 IDEG = SEC/3600.0
   IMIN = SEC/60.0-60.0*FLOAT(IDEG)
   SEC = SEC-3600.0*FLOAT(IDEG)-60.0*FLOAT(IMIN)
   ISEC = SEC
   SEC = SEC-FLOAT (ISEC)
   IF (SEC-0.9995) 60,45,45
45 SEC = 0.0
   ISEC = ISEC+1
   IF (ISEC-60) 60,50,50
50 ISEC = 0
   IMIN = IMIN+1
   IF (IMIN-60) 60,55,55
55 IMIN = 0
  IDEG = IDEG+1
60 LDX = ISI+ISS+1
   BEC=FLOAT (ISEC) +SEC
   ID=IDS(LDX)
   RETURN
   END
```

SUBROUTINE INEQZE(LAT, LON) DIMENSION LAT (999), LON(999) COMMON /55/DISS(999) COMMON /GROUND/ZDUM, Z, ZPDUM, ZP, XDUM, X, RO, DEN, R, U, OMX, WA 1VE, R2, ZPP, D, DOD1, DDD2 COMMON/INDUCT/WAY ZPP1, DINC1, TPI, NPTS COMMON/TE/TLA, TLON, RLAT, RLON, HLAT, HLON, 1.ZHAZ.WTH COMMON / ZOTA/ARRAY COMMON /SDRDI/S(999), DR(999), DI(999), LLM COMMON/CITCT/ITCT, LTOP, ALTT MSV COMMON/DELAY/NP, DISTSAV, TIMSAV DIMENSION ALTTHSV(3,2) DIMENSION E(999 , 2), F(999 , 2) DIMENSION ZZ(5), H(5) DIMENSION ZDUM(6), Z(1009), ZPDUM(6), ZP(1009), XDUM(6), X(1009), 1TZER(1), T(1000), GM(5), GX(5), EM(9), EX(9), MG(5), XS(9), ME(9), 2 W(1000), ARRAY (40), ZPP1(1089) COMPLEX O, DEN, DOD1, DDD2, FLEAF, F1, F2, F3, G1, G2, G3, SUM, TE 1RM, W, ME, MG, MM, MX COMPLEX TS, FIND, FINDH 2MAX), (ARRAY(11), FLAT) DATA IARRA/O/ DATA ((GX(K), K = 1, 5) = .02216356881, .1878315676, .4615973615, 1.7483346284, .9484939262) DATA ((GM(K), K = 1, 5) = .5910484494, .5385334386, .438172725, .2989026983, .1333426886) DATA ((EX(K), K = 1, 4) = .1051402826, .3762245145, .6989480124, 1 . 9373342493)

```
DATA ((EN(K), K = 1, 4) = .06568051989, .1960962655, .2525273456,
   1.1523625357)
     DATA (TZER(1)=1.0)
   FORMAT (//E20.7,5X, *ARRAY(1) = FRHZ = FREQUENCY IN KHZ*/
   1 E20.7.5X, FARRAY(2) = ETA = AIR INDEX OF REFRACTION AT GROUND*/
    2 E20.7,5X, FARRAY (3) = DMAX = MAXIMUM DISTANCE BETWEEN TRANSMITTER*
    3 ,* AND RECEIVER IN KH*/
      E20.7,5X, *ARRAY(4) = DINC = DISTANCE INCREMENT IN KH*/
      E20.7,5x, *ARRAY(5) = NSTART = INDEX OF THE FIRST DISTANCE AT*,
       * WHICH THE FIELD IS TO BE FOUND AS A FUNCTION OF ALTITUDE*/
      E20.7,5X, *ARRAY(6) = NZINC = THE FIELD IS TO BE FOUND AS A *,
      *FUNCTION OF ALTITUDE EVERY NZING INCREMENTS IN THE */
    9 40x, *DISTANCE ARRAY -- NZINC MUST NEVER BE LESS THAN 1*)
  7 FORMAT (E20.7,5X,*ARRAY(7) = INDEX OF THE LAST DISTANCE AT WHICH*,
    1 * THE FIELD IS FOUND AS A FUNCTION OF ALTITUDE*/
    2 E20.7,5%, *ARRAY(8) = ZMIN = THE MINIMUM ALTITUDE ABOVE THE *,
      *SURFACE AT WHICH THE FIELD IS FOUND, METERS*/
      E20.7,5X, *ARRAY(9) = ZINC = THE ALTITUDE INCREMENT, HETERS*/
      E20.7,5X, *ARRAY(10) = ZMAX = THE MAXIMUM ALTITUDE, METERS*/
    6 E20.7,5x, *ARRAY(11) = FLAT = THE FACTOR USED IN THE FLAT EARTH *,
    7 *TEST, METERS*/
    8 E20.7, 5x, *ARRAY(12) = ALPHA = VERTICAL LAPSE FACTOR*/
    9 E20.7,5x, *ARRAY(13) = EFFECTIVE EARTHS RADIUS*/
    A E20.7,5 X, *ARRAY (14) = NUT*//)
     IF (IARRA. 6T.1) GO TO 9999
     IARRA=2
     SET CONSTANTS
     NUT = ARRAY (14)
     RAD = 6.36739E+6 / ARRAY(12)
     ARRAY (13) = RAD
     FREQ = FKHZ * 1.E-3
     NSTART = ARRAY(5)
     NZINC = ARRAY(6)
     IF (ARRAY(6) .LT. 1.) NZINC = 1
     NZERO=0
     T(NZERO) =1.0
     WAVE = 2.095844729E-2 * FREQ
     HAVE = HAVE * ETA
     HAV= HAVE
     AMICRO = 1.0 / (TPI * FREQ)
     TX = SQRT(FREQ * ETA) * . 0408389549
     X(1) = 0.
     W(1) = 1.
9999 CONTINUE
     DECTX=X(2)
     DMAX=X(NPTS)/1000.
     DINC=DECTX/1000.
     ARRAY (4) =DINC
     DINC1=DINC
     ARRAY(7) = DMAX / DINC + 1.
     NZEND = ARRAY (7)
     PRINT 6, (AFRAY(I), I=1,6)
     PRINT 7, (ARRAY(I), I=7,14)
     NOFLAT = 1
     NG0 = 1
     D = CMPLX(DR(1), DI(1)) * SQRT(FREQ / 0.1)
    IMOST = DMAX / DINC + .01
DELTX = 1000. * DINC
     T(1) = 1. / SQRT (DELTX)
```

```
31 DO 32 K = 1, 5
     X( - K) = DELTX * GX(K)
     CALL GROUND ( -K, 2, 0, 0)
 32 MG(K) = FLEAF (WAVE, 0., 0., X( - K), D)
 37 CONTINUE
     ZPP=ZPP1(I)
     T(I) = 1. / SQRT(X(I) + DELTX)
OMX = OMCOS(X(I) / RAD)
     IGO = 2 - MOD(I, 2)
     IL = I - IGO - 1
     RD = SQRT(2. * RAD * (RAD + Z(I)) * ONX + Z(I) * * 2)
     GO TO (40, 45), NOFLAT IF (I .LE. 4 .OR. (FLAT .GT. X(I))) 41, 45
     H(I) = FLEAF(WAVE, 0., 0., X(I), D)
 41
     GO TO 90
     SUM = 0.
     NOFLAT = 2
 48 DO 50 K = 1, 5
CALL GEOM(I, - K, 1, 0.)

TERM = MG(K) * CMPLX(COS(WAVE * R), - SIN(WAVE * R)) * DEN

50 SUM = (U * GH(K)) / SQRT(X(I) - X( - K)) * TERM + SUM

SUM = 3. * T(1) * SUM
     KK = 1
     IF (IL .LT. 3) GO TO 100
DO 60 K = 3, IL
     CALL GEOMIT, K, 1, 0.)
     TERM = U * T(K - 1) * W(K) * CHPLX(COS (HAVE * R), SIN( - WAVE * R)
    1) * DEN
 GO TO (53, 55), KK
53 SUM = 4. * T(I - K) * TERM + SUM
     KK = 2
     GO TO 60
     SUM = 2. * T(I - K) * TERM + SUM
 55
     KK = 1
 60 CONTINUE
100 CONTINUE
     CALL GEOM(I, 2, 1, 0.)

SUM = T(I - 2) + T(1) + U + W(2) + CMPLX(COS(WAVE + R), - SIN(WAVE
    1 * R)) * DEN + SUN
 62 CALL GEOM(I, I - IGO, 1, 0.)
     F2 = U * T(TL) * W(I - IGO) * CMPLX(COS(HAVE * R), - SIN(WAVE * R)
    1) * DEN
     SUN = (SUM + T(IGO) * F2) * .333333333 * DELTX
      GO TO (65, 66), IGO
     F1 = F2
     F2 = TERM
      GO TO 70
 66 CALL GEOM(I, I - 1, 1, 0.)
F1 = U * T(I - 2) * W(I - 1) * CMPLX(COS(WAVE * R), - SIN(WAVE * R)
    1)) * DEN
     SUM = SUM + .0833333333 * DELTX * (5. * T(1) * F1 + 8. * T(2) * F
    12 - T(3) * TERM)
     Q = TX / T(I - 1)
      RHO = 1. + ZP(I)
     RHG = ZPP / RHO
 75 TERM = 1.2 / T(1) * T(T - 1) * CMPLX(Q, Q) * (D + CMPLX(0., - RHO
    1/ WAVE))
    WX = 1. - CMPLX(Q, Q) * (SUM + 2. / T(1) * (.466666667 * F1 - .066 1666667 * F2)) / (1. + TERM)
```

```
85 W(I) = WX
 90 DIST = .001 * X(I)
     CALL INDF(0., X(I), NUT, FIND)
     TS=W(I)*FIND
     AMP=CABS (TS)
     PHA= CANG (TS)
     PHIC = - (PHA - WAVE * (RO - X(I)))
     SEC = PHIC * AMICRO
     IF (I. NE. NP) 50 TO 9876
      DISTSAV=DIST
      TIMSAV=SEC
9876 CONTINUE
      I = I + 1
      IF (I.LE. NPTS) GO TO 37
150 NGO = 2
     IF (ZMAX.LE.G.) RETURN
IFOP = (NZEND - NSTART) / NZINC + 1
     IF (ITOP .GT. 1500) GO TO 280
     LTOP= (ZMAX-ZMIN) /ZINC+1.1
      IF (LTOP. GT.5) GO TO 280
     F2=(0.,0.)
     G2=(0.,0.)
     OLDR=0.
     IF (ITCP .LT. 1) GO TO 105
       NPALT=NP-NSTART+1
     DO 200 IS = 1, ITOP
     I = NSTART + (IS - 1) * NZINC
     II=I
     IF (I.GE.NZEND) II=NZEND-1
     IGO = 2 - MOD(I, 2)
     DO 155 K = 1, 4
X(1000 + K) = X(I) - DELTX * EX(K)
      XS(K) = X(1000 + K)
 155 CALL GROUND (1000+K, II, 0, 0)
CALL CNEVKEN(X, W, IMOST, XS, WE, 4, 5, 1)
      IF (LTOP .LT. 1) GO TO 110
     DO 195 L = 1, LTOP
H(L) = ZMIN + (L - 1) * ZINC
      IF (H(L) .LT. Z(I)) 156, 154
156 WW = 0.
      GO TO 193
154 ZZ(L) = RAD + H(L)
      RO = SQRT(2. * RAD * ZZ(L) * OHCOS(X(I) / RAD) + H(L) * * 2)
      SUM = 0.
      DO 157 K = 1, 5
      CALL GEOM(I, - K, 2, H(L))
TERM = HG(K) * CHPLX(COS(WAVE * R), - SIN(WAVE * R)) * DEN
157 SUM = U * GH(K) * TERM / SQRT(X(I) - X( - K)) + SUM
      SUM = 3. * T(1) * SUM
     CALL GEOM(I, 3, 2, H(L))

F1 = T(1) * T(I - 2) * U * DEN * W(2)

G1 = CMPLX(COS(WAVE * R), - SIN(WAVE * R))
     SUM = SUM + F1 * G1
ILO = I - IGO
      KG0 = 1
      IF (ILC .LT. 3) GO TO 115
      DO 182 K = 3, ILO
      F3 = F2
      G3 = G2
      F2 = F1
```

```
62 = 61
       CALL GEOM(I, K, 2, H(L))
       G1 = CMPLX(COS(WAVE * R), - SIN(WAVE * R))

F1 = T(K - 1) * T(I - K) * U * DEN * W(K)
       DELTG = WAVE * (R - OLDR)
GO TO (158, 159, 172), KGO
158 SUM = SUM + 4. * F1 * G1
       KG0 = 2
       GO TO 182
       SUM = SUM + 2. * F1 * G1
       KG0 = 1
       IF (A8S(DELTG) .GT. .2) 170, 182
      KG0 = 3
       SUM = SUM - F1 * G1
       GO TO 182
172 SUM = SUM + CMPLX(0., 3. / DELTG) * (G1 * (F1 - .5 * (F1 * CMPLX(2 1., 3. * DELTG) - 4. * F2 * CMPLX(1., DELTG) + F3 * CMPLX(2., DELTG 2)) / DELTG * * 2) - G2 * (F2 - .5 * (F1 * CMPLX(2., DELTG) - 4. *
      3F2 + F3 * CMPLX(2., - DELTG)) / DELTG * * 2))
182 OLDR = R
115 CONTINUE
       GO TO (188, 183), IGO
       F3 = F2
183
       63 = 62
       F2 = F1
       62 = 61
       CALL GEOM(I, I - 1, 2, H(L))
G1 = CMPLX(COS(MAVE # R), - SIN(MAVE # R))
F1 = T(I - 2) # T(1) # U # DEN # W(I - 1)
       DELTG = FAVE * (R - OLDR)
       IF (ABS(DELTG) .GT. .2) 184, 185
     SUM + CMPLX(0., 3. / DELTG) * (G1 * (F1 - .5 * (F1 * CMPLX(2 1., 3. * DELTG) - 4. * F2 * CMPLX(1., DELTG) + F3 * CMPLX(2., DELTG 2)) / DELTG * * 2) - G2 * (F2 - .5 * (F1 * CMPLX(2., DELTG) - 4. * 3F2 + F3 * CMPLX(2., - DELTG)) / DELTG * * 2))
       GO TO 188
185 SUM = SUM + 1.25 * F1 * G1 + 2. * F2 * G2 - .25 * F3 * G3
       DO 190 K = 1, 4
       CALL GEOP(I, 1000 + K, 3, H(L))
SUM = SUM + 3. * EN(K) * NE(K) * CMPLX(COS(WAVE * R), - SIN(WAVE *
      1 R)) * DEN * U / (SQRT (XS (K)) * T(1))
190 CONTINUE
        SUM = .33333333 * DELTX * SUM
Q = TX / T(I - 1)
HH = (1. - CMPLX(Q, Q) * SUM) * .5
193
       CONTINUE
        CALL INDF (H(L), X(I), NUT, FINDH)
        TS=WWFINDH
        E(IS, L) = CABS(TS) + 1.257 + FREQ / RO
        F(IS, L) = - (CANG(TS) - WAVE + (RO - X(I)))
195 CONTINUE
 110
       CONTINUE
        DISS(IS) = .001 + x(I)
200
       CONTINUE
105
       CONTINUE
        IF (LTOP .LT. 1) GO TO 120
        DO 250 L = 1, LTOP
IF (ITCP .LT. 1) GO TO 125
        DO 240 IS = 1, ITOP
```

```
FM = F(IS, L) * AMICRO
IF(IS.NE.NFALT) GO TO 9877
ALTTMSV(ITCT,L) = FM

9877 CONTINUE
240 CONTINUE
125 CONTINUE
250 CONTINUE
120 CONTINUE
280 CONTINUE
RETURN
END
```

```
SUBROUTINE GROUND(I, K, IGO, HH)
COMMON /GROUND/ZDUM, Z, ZPDUM, ZP, XDUM, X, RO, DEN, R, U, OMX, HA
    IVE, R2, 2PP, DELTA, DELTA1, DELTA2
COMMON / 20TA/ARRAY
     COMMON /SDRDI/S(999), DR(999), DI(999), LLM
     DIMENSION ZDUM(6), Z(1009), ZPDUM(6), ZP(1009), XDUM(6), X(1009),
    1ARRAY (40)
     COMPLEX DELTA, DEN, DELTA1, DELTA2
     EQUIVALENCE (ARRAY(1), FKHZ), (ARRAY(13), A)
     CALL INT (K,I)
     FREQ = FKHZ * 1.E-3
     RETURN
     ENTRY GEOM
     HIT = Z(I) + HH
     IF (I .EQ. K) GO TO 20
     T = (X(I) - X(K)) / A
     GS = A + Z(K)
     GX = A + HIT
     CT = COS (T)
     ST = SIN(T)
     OT = OMCOS(T)
     R2 = SQRT(2. + GS + GX + OT + (HIT - Z(K)) + 2)

R1 = SQRT(2. + A + GS + DMCOS(X(K) / A) + Z(K) + 2)
     R = R1 + R2 - R0
     U = X(K) + R0 + SQRT(1 + ZP(K) + 2) / (R1 + R2 + X(I))
     IF (IGC .LT. 3) U = U + (X(I) - X(K))
PD = (A + OT + Z(K) - HIT + CT + GX + ZP(K) + A + ST / GS) / R2
     XK = X(K)
     IF (XK .GE. S(LLM)) GO TO 12
     LLL = 1
     IF (XK .LT. S(1)) GO TO 10
     LLMO = LLM - 1
     IF (LLMO .LT. 1) GO TO 100
     DO 13 LLL = 1, LLMO
     IF (XK .LT. S(LLL + 1) .AND. XK .GE. S(LLL)) GO TO 10
13 CONTINUE
100 CONTINUE
     GO TO 21
10 DELTA = CMPLX(DR(LLL), DI(LLL)) * SQRT (FREQ / 0.1)
 12 DELTA = CMPLX(DR(LLM), DI(LLM)) * SQRT(FREQ / 0.1)
 21 CONTINUE
     DELTA2 = CMPLX(1., - 1. / (MAVE * R2)) * PD
     DELTA1 = DELTA - DELTA2
 19 DEN = DELTA2 + DELTA
     RETURN
```

20 U = 0. R2 = GX - A - Z(I) RETURN END

SUBROUTINE GETELV(LATX, LONX, AMP, FAZ, EL VTN) COMMON/GETELV/L(120),IMP(120) COMMON/UNPACK/NPACK(60) \$COMMON/FLAGS/IXPT, NFLAG DIMENSION MSINDX(5800) DATA KPS1/1/ INDDIM=5800 IF (KPS1.EQ.1) CALL OPENMS (2, MSINDX, INDDIM, 0) \$KPS1=0 M11=37778\$M8=3778 IF(LATX-LT-480000 .OR. LATX-GE-54000) GO TO 190 IF(LONX-LT-060000 .OR. LONX-GE-140000) GO TO 190 NFL AG=0 \$L ATSEC=MOD (L ATX, 100) \$L ONSEC=MOD (L ONX, 100) LATDM=LATX-LATSEC\$LONDM=LONX-LONSEC\$IF (LATSEC.GE.30)GOTO40 LATS=LATDM\$LATN=LATDM+30\$GO TO 60 40 LATS=LAT DM+30 \$LATN=LATDM+100 \$LATM=MOD(LATDM,10000) IF (LATM. EQ. 5900) LATN=LAT DM+4100 60 IF (LONSEC. GE. 30) GOTO80 \$LONN=LONDM\$LONE=LONDM+30\$GOTO100 80 LONW=LONDM+30\$LONE=LONDM+100 LONM= MOD (LONDH, 10000) IF (LONM. EG. 5900) LONE = LONDM+4100 100 CONTINUE INDNE=INDEX(LATN, LONE) IF (NFLAG. EQ.1) GO TO 120 CALL READMS(2, NPACK, 60, INDNE) CALL UNPACK INE=L(IXPT) IF (MOD (LATH, 10000) . EQ. 0. OR. MOD (LONE, 20000) . EQ. 0) GOTO120 ISE=L(IXPT-1) CALL READMS (2, NPACK, 60, INDNE-1) \$CALL UNPACK INW=L(IXPT) \$ISW=L(IXPT-1) \$GO TO 180 120 CONTINUE INDNW=INDEX(LATN, LONW) IF(NFLAG.EG.1) GO TO 140 CALL READMS (2, NPACK, 60, INDNW) CALL UNPACK INW=L (IXPT) 140 CONTINUE INDSE=INDEX(LATS, LONE) IF (NFLAG. EQ.1) GO TO 160 CALL READMS (2, NPACK, 60, INDSE) CALL UNPACK ISE=L(IXPT) 160 CONTINUE INDSH=INCEX(LATS, LONM) IF(NFLAG.EG.1) GO TO 180 CALL READMS (2, NPACK, 60, INDSW) CALL UNPACK ISH=L (IXPT) 180 CONTINUE AMP=FLCAT(SHIFT(IMP(IXPT),-11).A.M8)*.001 FAZ=FLOAT (IMP(IXPT) . A. M11) *. 001 IF(NFLAG.EG.1) PRINT 3100

ELEAST=FLOAT(ISE)+FLOAT((INE-ISE)*(LATSEC-(LATSEC/30)*30))/30.
ELWEST=FLOAT(ISM)+FLOAT((INM-ISM)*(LATSEC-(LATSEC/30)*30))/30.
ELWTN=ELWEST+(ELEAST+ELWEST)*FLOAT(LONSEC-(LONSEC/30)*30)/30.
RETURN
190 PRINT 2070
RETURN

2070 FORMAT (* *,4H****,*LAT,LON REQUESTED ARE OUTSIDE MAP REGION - NO E 1LEVATION RETURNED*,//)
3100 FORMAT (* *,4H****,*INDEX REQUESTED EXCEEDS SCANLINES GENERATED, TH 1US PREVIOUS ELEVATIONS WILL BE USED*)

FIND

FUNCTION INDEX (LAT, LON) COMMON/FLAGS/IXPT, NFLAG LATS=MOD (LAT, 100) LATH=HOD (LAT, 10000) -LATS LATD= (LAT-LATH-LATS) /10000 LATH=LATH/100 LONS=HOD (LON, 100) LONM=HOD (LON, 10000) -LONS LOND= (LO 1-LONH-LONS) /1000 8 LONM=LONM/100 ISUBL N=(LOND*5) ISUBLN=(MOD(ISUBLN,10)/5)*120 ILOND= ((LOND-6)/2) #1448+ISUBLN+LONM#2+LONS/38+1 INDEX=ILONO+(LATD-48) #248 IXPT=LATH#2+LATS/30+1 IF (INDEX. GT.5760) NFL AG=1 RETURN END

SUBROUTINE UNPACK
CDMMON/GETELV/L (120), IMP(120)
COMMON/UNPACK/NPACK (60)
DATA MSK1/3777B/, MSK2/1777777B/
DD 20 MA±1,60\$M=2*(MA-1)+1
L(M)=AND (MSK1, SHIFT (MPACK (MA), -49))*8
IMP(M)=AND (MSK2, SHIFT (MPACK (MA), 30))
L(M+1)=AND (MSK1, SHIFT (MPACK (MA), -19))*8
IF(L(M).GT.2000)L(M)=96\$IF(L(M+1).GT.2000)L(M+1)=96
IMP(M+1)=AND(MSK2, MPACK (MA))
20 CONTINUE\$END

```
SUBROUTINE GEODI(B1, AL1, AZ12, S, B2, AL2, AZ21)
C----CALCULATES INVERSE COMPUTATION FORM (SODANO, 1965)
C----B1, AL1, B2, AL2 ARE GIVEN DATA
C----AZ12,S,
                AZZ1 ARE CALCULATED DATA
C-----B1 = GEODETIC LATITUDE, RADIANS, OF FIRST POINT
C----AL1 = GEODETIC LONGITUDE, RADIANS, OF FIRST POINT
C-----B2 = GEODETIC LATITUDE, RADIANS, OF SECOND POINT
C----AL2 = GEODETIC LONGITUDE, RADIANS, OF SECOND POINT
C----AZ12 = FORWARD AZIMUTH, RADIANS, FROM FIRST POINT
C----AZ21 = BACK AZIMUTH, RADIANS, FROM SECOND POINT
C----S = DISTANCE (LENGTH OF GEODETIC LINE) BETWEEN POINTS, METERS
C----SOUTHERN LATITUDES AND WESTERN LONGITUDES ARE NEGATIVE
      COMMON /GENERAL/TPI, PI, PI2, PI4, AO, BO, FL, ESQ, IFLAG
      DATA (IFLAG = 1)
      IF (IFLAG .EQ. 1) CALL SETULIF (ABS(B1) .GT. PI4) GO TO 1
TBET1 = TAN(B1) * (1. - FL)
                           CALL SETUP
      BET1 = ATAN(TBET1)
      GO TO 2
   1 CBET1 = 1.0 / TAN(B1) / (1. - FL)
      BET1 = ATAN(1. / CBET1)
   2 CONTINUE
      ALL1 = AL2 - AL1
      IF (AL2 - AL1 .EQ. 0.) 8, 9
      ALL2 = 0.
      GO TO 3
   9 CONTINUE
      ALL2 = AL2 - AL1 - SIGN (TPI, AL2 - AL1)
   3 IF (ABS(ALL1) .GT. ABS(ALL2)) 5, 6
   5 ALL = ALL2
      60 TO 7
      ALL = ALL1
      CONTINUE
  12 IF (ABS(ALL) .EQ. 0. .OR. ABS(ALL) .EQ. PI .OR. ABS(ALL) .EQ. TPI)
    1 10, 11
     ALL = ABS (ALL)
  11 CONTINUE
      IF (ABS(B2) .GT. PI4) GD TO 16
TBET2 = TAN(B2) * (1. - FL)
      BET2 = ATAN(TBET2)
      GO TO 17
  16 CBET2 = 1.0 / TAN(82) / (1. - FL)
      BET2 = ATAN(1. / CBET2)
  17 CONTINUE
      CBET1 = COS(BET1)
      SBET1 = SIN(BET1)
      CBET2 = COS(BET2)
      SBET2 = SIN(BET2)
      A = SBET1 * SBET2
B = CBET1 * CBET2
      AB = SBET1 * CBET2
      BA = SBET2 * CBET1
      COSL = COS(ALL)
      SINL = SIN(ALL)
      CPHI = A + B * COSL
SPHI = SQRT ((SINL * CBET2)**2 + (BA - AB * COSL)**2)
      IF (SPHI .GE. C. .AND. CPHI .GE. 0.) 20, 21
```

```
20 PHI = ASIN(SPHI)
    IF (SPHI .GT. CPHI) PHI = ACOS (CPHI)
    GO TO 30
    IF (SPHI .GE. 0. .AND. CPHI .LE. 0.) 22, 23
PHI = PI - ASIN(SPHI)
21
    IF (SPHI .GT. ABS(CPHI)) PHI = ACOS(CPHI)
GO TO 30
23 IF (SPHI .LT. 0. .AND. CPHI .LT. 0.) 24, 25
    IF (ABS(SPHI) .GT. ABS(CPHI)) PHI = TPI - ACOS(CPHI)
    GO TO 30
25 IF (SPHI .LT. 0. .AND. CPHI .GE. 0.) 26, 27
26 PHI = TPI + ASIN(SPHI)
    IF (ABS(SPHI) .GT. CPHI) PHI = TPI - ACOS(CPHI)
    GD TO 30
27
    CALL EXIT
    CONTINUE
    C = B * SINL / SPHI
    FL2 = FL * FL
    CON1 = FL + FL2
    CON2 = 0.5 * FL2
    CON3 = SPHI * CPHI
    CON4 = PHI ##2 / SPHI
    CONS = CON4 * CPHI
    EN = 1. - C * * 2
    RATIO1 = (1. + CON1) * PHI + A * (CON1 * SPHI - CON2 * CON4)
   1 + EM * (-0.5 * CON1 * (PHI + CON3) + CON2 * CON5) - A * A * CON2
2 * CON3 + EM * EM * CON2 * (0.125 * (PHI + CON3) - CON5 + 8.25 *
    3 CON3 * CPHI**2) + A * EM * CON2 * (CON4 + CON3 * CPHI)
    S = RATIO1 * 80
    IF (S .LE. 1.E-4) S = 0.

RATIO2 = CON1 * PHI - A * CON2 * (SPHI + 2. * CON4)
   1 + 0.5 * EM * CON2 * (-5.0 * PHI + CON3 + 4.0 * CON5)
    ALAM = RATIO2 * C + ALL
    SALAM = SIN(ALAM)
    CALAM = COS(ALAM)
    CTAZ12 = 8A - CALAM * AB
    CTAZZ1 = BA * CALAM - AB
    IF (AL1 - AL2 .EQ. 0.)
                               35, 39
35 AZ12 = 0.
    AZ21 = 0.
    GO TO 34
39 CTAZ12 = CTAZ12 / (SALAM * CBET2)
    IF (CTAZ12 .EQ. 0.) 54, 55
    AZ12 = PI2
    GO TO 56
55 CONTINUE
     AZ12 = ATAN(1. / CTAZ12)
56 CONTINUE
    CTAZ21 = CTAZ21 / (SALAN * CBET1)
    IF (CTAZ21 .EQ. 0.) 57, 58
57 AZ21 = PI2
    GO TO 34
58 CONTINUE
     AZ21 = ATAN(1. / CTAZ21)
34 CONTINUE
     IF (ALL .GE. 0. .AND. CTAZ12 .GE. 0.) 40, 41
```

```
40 AZ12 = AZ12
GO TO 50
41 IF (ALL .GE. 0. .AND. CTAZ12 .LT. 0.) 42, 43
42 AZ12 = PI + AZ12
GO TO 50
43 IF (ALL .LT. 8. .AND. CTAZ12 .GE. 8.) 44, 45
44 AZ12 = PI + AZ12
    GD TO 50
45 AZ12 = TPI + AZ12
58 IF (ALL .6E. 0. .AND. CTAZ21 .GE. 0.) 46, 47
46 AZ21 = PI + AZ21
    60 TO 51
47 IF (ALL .GE. 0. .AND. CTAZ21 .LT. 0.) 48, 49
48 AZ21 = TPI + AZ21
    60 TO 51
49 IF (ALL .LT. 0. .AND. CTAZZ1 .GE. 0.) 52, 53
52 AZ21 = AZ21
    60 TO 51
53 AZ21 = PI + AZ21
51 CONTINUE
    AZ12 = AMOD(AZ12, TPI)
    IF (AZ12 eLT. 0.) AZ12 = AZ12 + TPI
AZ21 = AMOD(AZ21, TPI)
    IF (AZ21 .LT. 0.) AZ21 = AZ21 + TPI
    RETURN
    END
```

SUBROUTINE SETUP

COMMON /GENERAL/TPI, PI, PI2, PI4, A0, B0, FL, ESQ, IFLAG

DATA (TPI=6.28318530717959)

PI = TPI / 2.8

PI2 = TPI / 4.0

PI4 = TPI / 8.8

C-----A0=SEMIMAJOR AXIS OF CLARKE SPHEROID OF 1866, METERS

C-----B8=SEMIMINOR AXIS OF CLARKE SPHEROID OF 1866, METERS

A0 = 6.3782064E+6

B0 = 6.3782064E+6

C-----FL=SPHEROIDAL FLATTEMING

C-----ESQ=SECOND ECCENTRICITY SQUARED

FL = 1.0 - B0 / A0

ESQ = (A0 ** 2 - B0 ** 2) / B0 ** 2

IFLAG = 0

RETURN

END

FUNCTION OMCDS (X) C OMOCOS(X) = 1 - COS(X)IF (ABS(X) .GT. .15) GO TO 40 IF (X .EQ. 0.) GO TO 50 S = X * X OMCOS = T = .5 * S R = 4. 10 T = - T * S / (R * (R - 1.)) ONCOS = CMCOS + T IF (T / OMCOS .LE. .5E-9) GO TO 51 R = R + 2. 60 TO 10 40 OMCOS = 1. - COS(X) RETURN 50 OMCOS = 0. 51 RETURN END

SUBROUTINE INT (I,K) I = POSITION IN X AND Z ARRAYS ON WHICH TO CENTER CALCULATIONS K = POSITION IN ARRAYS Z AND ZP TO STORE CALCULATED VALUES COMMON /GROUND/ ZDUM, Z, ZPDUM, ZP, XDUM, X, RO, DEN, R, U, OMX, WAVE, R2, ZPP 1,0,0001,0002 COMPLEX DEN,D, DDD1, DDD2 DIMENSION ZDUM(6), Z(1009), ZPDUM(6), ZP(1009), XDUM(6), X(1009) IMO=I-1 IP0=I+1 C = ((Z(IPO) - Z(IMO)) - (Z(I) - Z(IMO)) * (X(IPO) - X(IMO)) / (X(I) - X(IMO)))/1 ((X(IPO)*X(IPO)-X(IMO)*X(IMO))-(X(I)*X(I)-X(IMO)*X(IMO))* 2 (X(IPO)-X(IMO))/(X(I)-X(IMO))) B = ((Z(I) - Z(IMO)) - C + (X(I) + X(I) - X(IMO) + X(IMO))) / (X(I) - X(IMO))A= Z(I)-X(I)*(B+C*X(I)) Z(K) = A + X(K) + (B + C + X(K))ZP(K)=B+2. *C*X(K) ZPP=2. C RETURN END

SUBROUTINE CHEVKEN(A, FA, NA, X, FX, NX, NPT, KASE) COMPLEX FA, FX, FUNCT, POLY DIMENSION A(NA), FA(NA), X(NX), FX(NX), FUNCT(15), ABSC(15), DIF(1 15), POLY(15) 1 FORMAT (1H1/50H THE X VALUES ARE NOT ARRANGED IN ASCENDING ORDER./ 1/5X,4HI = E20.9,5X,7HX(I) = E28.9,5X,4HJ = E20.9,5X,7HA(J) = E20.9 2///14X,1HX,20X,4HF(X)) 2 FORMAT (5x, 2E20.9) 200 FORMAT (1H1* THERE ARE NOT ENOUGH POINTS IN THE GIVEN ARRAY. *)
205 FORMAT (1H1* THE GIVEN VALUE OF NPT WAS GREATER THAN NA. */* THE SU 1BROUTINE REDUCED NPT TO WITHIN THE LIMITS OF NA. +) 210 FORMAT (1H1* NPT WAS INITIALLY GREATER THAN 15 - NPT =15. 4/4 THE S 1UBROUTINE SET NPT TO 15 AND CONTINUED. *) L00P = 1 IF (NPT - 15) 3, 3, 9 9 PRINT 210, NPT NPT = 15

```
3 IF (NPT - NA) 8, 8, 4
     NPT = NPT - 2
      IF (NPT - 1) 5, 5, 6
     PRINT 200
      CALL EXIT
     60 TO (7, 3), LOOP
     LOOP = 2
      PRINT 205
      GO TO 3
     NPT2 = NPT / 2
      GO TO (11, 12), KASE
 11 NSTART = 1
      MX = 1
      60 TO 16
12 NSTART = NA - 3
      TEST = A(NSTART) + (A(NSTART + 1) - A(NSTART)) / 2
      IF (NX .LT. 1) GO TO 170
      DO 14 I = 1, NX
      IF (X(I) - TEST) 14, 14, 13
 13 MX = I
      GO TO 16
     CONTINUE
     CONTINUE
170
      NSTOP = NA - 1
 16
      IF (NX .LT. MX) GO TO 175
    DO 125 I = MX, NX
IF (X(I) - A(1)) 135, 15, 10
IF (X(I) - A(NA)) 25, 20, 130
 10
 15 FX(I) = FA(1)
      GO TO 125
     FX(I) = FA(NA)
 20
      60 TO 125
     IF (NSTOP .LT. NSTART) GO TO 180
DO 85 J = NSTART, NSTOP
     IF (X(I) - A(J)) 32, 35, 30
IF (X(I) - A(J + 1)) 45, 40, 85
 32 II = I - 1
     PRINT 1, I, X(I), J, A(J)
IF (II) 34, 34, 33
PRINT 2, (X(N), FX(N), N = 1, II)
      CALL EXIT
 34
 35
      FX(I) = FA(J)
      NSTART = J
      GO TO 125
FX(I) = FA(J + 1)
      NSTART = J + 1
     GD TO 125
NSTART = J
      IF (ABS(X(I) - A(J)) - ABS(X(I) - A(J + 1))) 50, 50, 55
 50
      JJ = J
      GO TO 60
     JJ = J + 1
      GO TO 60
 85 CONTINUE
180
      CONTINUE
 60 IF (JJ - NPT2) 135, 135, 70
70 IF (JJ + NPT2 - NA) 80, 80, 130
80 KK = JJ - NPT2 - 1
```

```
90 IF (NPT .LT. 1) GO TO 185
     DO 95 K = 1, NPT
     KK = KK + 1
     FUNCT(K) = FA(KK)
     ABSC(K) = A(KK)
 95 DIF(K) = ABSC(K) - X(I)
185
     CONTINUE
     NTOP = NPT - 1
LL = 1
100 IF (NTOP .LT. 1) GO TO 190
     DO 105 L = 1, NTOP
     LLL = L + LL
105 POLY(L) = (FUNCT(L) * DIF(LLL) - FUNCT(L + 1) * DIF(L)) / (ABSC(LL
    1L) - ABSC(L))
190 CONTINUE
     IF (NTOP - 1) 120, 120, 110
110 DO 115 M = 1, NTOP
115 FUNCT (N) = POLY(N)
     NTOP = NTOP - 1
LL = LL + 1
     GO TO 100
    INC = - 1
130
     KK = NA + 1
     60 TO 148
135 INC = 1
     KK = 0
140 IF (NPT .LT. 1) GO TO 215
     DO 145 K = 1, NPT
KK = KK + INC
     FUNCT(K) = FA(KK)
     ABSC(K) = A(KK)
145 DIF(K) = ABSC(K) - X(I)
215
     CONTINUE
     NTOP = NPT - 1
LL = 1
150 IF (NTOP .LT. 1) GO TO 220
     DO 155 L = 1, NTOP
     LLL = L + LL
155 PDLY(L) = (FUNCT(1) * DIF(LLL) - FUNCT(L + 1) * DIF(LL)) / (ABSC(L
    1LL) - ABSC (LL))
220 CONTINUE
     IF (NTCP - 1) 120, 120, 160
160 DO 165 M = 1, NTOP
165 FUNCT(M) = POLY(M)
     NTOP = NTOP - 1
     LL = LL + 1
GO TO 150
     FX(I) = POLY(1)
120
     CONTINUE
125
175
     CONTINUE
     RETURN
     END
```

```
COMPLEX FUNCTION FLEAF (HAVE, H1, H2, XD, DELTAR)
 COMPLEX TEMP, Q, Z, ZZ, ZZ, HWERF, WERFZ, WERF, ZWERF, DELTAR
HD = H2 - H1
TEMP = (0.7071067812, - 0.7071067812) * SQRT(.5 * WAVE)
XD2 = SQRT(XD)
 Q = - TEMP * HD / XD2
 Z = TEMP * DELTAR * XD2 + Q
 ZZ = - Z
ZI = AIMAG(ZZ)
 IF (ZI .LT. 0. .OR. (ABS(REAL(ZZ)) .LT. 6. .AND. ZI .LT. 6.)) GO T
10 10
22 = 22 + + 2
HWERF = (72 - 2.) / (77 * (72 - 3.5))
GO TO 12
 HERF - COMPLEMENTARY ERROR FUNCTION
WERFZ = WERF(ZZ)
HWERF = ZZ - 0.5 * WERFZ / (ZZ * WERFZ + (0., - 0.56418958))
ZWERF = Z + HWERF
FLEAF = (Q * ZWERF - 0.5) / (Z * ZWERF - 0.5)
RETURN
 END
```

```
COMPLEX FUNCTION WERF (ZZZ)
COMPLEX Z, ZZZ, ZV, V, ZZ, C, N, S
DIMENSION C(12), W(5, 4)
EQUIVALENCE (S, C(12))
DATA (C(1) = (.0, - .5641895835))
DATA W/(1.,0.0),
1 (3.678794411714423E-01,6.071577058413937E-01),
2 (1.831563888873418E-02,3,400262170660662E-01),
3 (1.234098040866788E-04,2.011573170376004E-01),
4 (1.125351747192646E-07,1.459535899001528E-01),
5 (4.275835761558070E-01,0.0000000000000000E+00),
6 (3.047442052569126E-01,2.082189382028316E-01),
7 (1.4023 9581366277 9E-01, 2.222134401798 991E-01),
8 (6.531777728904697E-02,1.739183154163490E-01),
9 (3.628145648998864E-02,1.358389510006551E-01),
A (2.553956763105058E-01,0.000000000000000E+00),
B (2.1849 26152748907E-01,9.299780939260186E-02),
C (1.479527595120158E-01,1.311797170842178E-01),
D (9.271076642644332E-02,1.283169622282615E-01),
E (5.968692961044590E-02,1.132100561244882E-01),
G (1.642611363929861E-01,5.019713513524966E-02),
H (1.307574696698522E-01,8.111265047745472E-02),
I (9.640250558364439E-02,9.123632600421258E-02),
J (6.979096164964750E-02,8.934000024036461E-02)/
XX = REAL (ZZZ)
 YY = AIMAG(ZZZ)
 X = ABS(XX)
 Y = ABS(YY)
 Z = CMPLX(X. Y)
 LZ2 = 0
 IF (X .GE. 4.5 .OR. Y .GE. 3.5) GO TO 100
I = X + .5
 J = Y + .5
 V = CMPLX(FLOAT(I), FLOAT(J))
```

```
zv = z - v
      C(2) = H(I + 1, J + 1)
      AI = 0.
      DO 10 I = 3, 12
AI = AI - .5
C(I) = (V * C(I - 1) + C(I - 2)) / AI
 10 CONTINUE
      J = 12
      DO 11 I = 2, 11
      J = J - 1
11 S = S * ZV + C(J)
20 IF (YY .GE. 0.) GO TO 30

IF (LZ2 .EQ. 0) Z2 = Z * Z

S = 2. * CEXP( - Z2) - S

IF (XX .GT. 0.) S = CONJG(S)
      GO TO 200
    IF (XX .LT. 0.) S = CONJG(S)
WERF = S
200
      RETURN
100 LZ2 = 1
      zz = z + z
      S = Z * ((0., 0.4613135279) / (Z2 - 0.1901635092) + (0., 0.0999921
    16168) / (22 - 1.7844927485) + (0., 0.0028838938748) / (22 - 5.5253
     243743791)
      GD TO 20
      END
```

```
FUNCTION CANG(Z)
   COMPLEX Z
   DATA (PI=3.14159265358979), (PIHA=1.57079632679489)
   X=REAL(Z)
   Y=AIMAG(Z)
   IF (X) 26,30,10
10 CANG=ATAN2 (Y, X)
   RETURN
20 IF (Y.NE.O.)
                 GO TO 10
   CANG=PI
   RETURN
                  GO TO 40
30 IF (Y.GT.O.)
   IF (Y.LT.0.)
                  GO TO 50
   CANG=0.
   RETURN
4C CANG=PIHA
   RETURN
50 CANG=-PIHA
   RETURN
   END
```

```
SUBROUTINE INDF (HH, XX, NUT, F)
THIS SUBROUTINE CALCULATES THE INDUCTION FIELDS FOR E SUB R AND
      H SUB PHI
C
      THESE INDUCTION FIELDS ARE FOR POSITIVE TIME FUNCTION
      NUT = 1 GIVES INDUCTION FIELD FOR E SUB R (TAU BAR)
      NUT = 0 GIVES INDUCTION FIELD FOR H SUB PHI (LOOP)
      FZ = INDUCTION FIELD FOR E SUB R
FH = INDUCTION FIELD FOR H SUB PHI
C
      COMMON/INDUCT/WAVE
      DOUBLE THETAD, SINTH, COSTH, R, CONS
COMPLEX GZ, FZ, FH, F
      A=6.36739 E6
      TPI=6.283185307
      C=2.997925E8
      IF(XX.LE.0.)3,4
      PRINT 5
    5 FORMAT (//* IN INDF, DISTANCE IS ZERO OR NEGATIVE, XX = *, E20.10)
      CALL EXIT
    4 THETAD=1.D8*XX/A
      SINTH=OSIN (THETAD)
      COSTH=DCOS (THETAD)
       R=A+HH
      CONS=A*R*SINTH**2
      D2=R#R+A#A-2. #A#R#COSTH
      IF (02.6T.0.) GO TO 30
      DD=XX
      D2=XX*XX
       GO TO 40
   30 CONTINUE
      DD=SQRT(D2)
   48 CONTINUE
      03=00*02
      D4=D2*D2
       FZR=-2.*COSTH/DD+3.*CONS/D3
       FZI= (WAVE+CONS+2. +COSTH/WAVE)/DZ-3. +CONS/(D4+WAVE)
      FZ=CHPLX(FZR,FZI)
      GZ=CMPLX (0., MAVE)
       FZ=FZ/GZ
      FHR=R*SINTH*DD/D3
      FHI = WAVE *R*SINTH*DO/D2
       FH=CMPLX (FHI,-FHR)
      C1=2.E-7*TPI*WAVE*C
      FH=FH/C1
      IF (NUT)1,2
    1 F=FZ
      RETURN
    2 F≈FH
      RETURN
       END
```

3.7 Sample Test Run

A typical data output listing is illustrated below. The transmitter coordinates which are read in from the data card deck are printed for verification purposes. The geographic coordinates of the desired target or receiver are next listed. Array data used in the calculations are then printed. TOA is the travel time from transmitter to receiver in µsec and recorded in order of master, slave 1 and slave 2 to

target respectively. TD1 and TD2 are the final desired LORAN coordinates in μ sec. ED1 and ED2 are the slave emission delays in μ sec obtained from the transmitter card input data. Additional output data recorded as TOA above include:

DISTDUM - Calculation of distance by Hufford's technique in KM.

TIMDUM - Calculation of secondary phase factor in µsec.

DISTSOD - Calculation of distance by Sodano technique in KM.

TPW - Travel time of primary wave in μsec.

3.8 Output Listing

LOCATION	LATITUDE	LONGITUDE
	(DEG-MIN-SEC)	(DEG-MIN-SEC)
MASTER	49 36 18.813N	7 19 38.2755
SLAVE1	53 39 13.867N	8 43 47.5 95
SLAVE2	48 15 48.929N	11 37 49.263E
PECET VER COOPDI	NATES	AND THE PROPERTY AND TH
LOCATION	LATITUDE	LONGITUDE
	(DEG-MIN-SEC)	(DEG-MIN-SEC)
RECTIVER 5	50 31 29.176N	8 37 4.1025
10000 noE+03	ARRAY(1) = FKHZ = FREQUENCY	IN KHZ
1000738E+01	ARRAY(2) = ETA = AIR INDEX O	F REFRACTION AT GROUND
3751978E+03	ARRAY(3) = DMAX = MAXIMUM DI	
95761 24E+00	ARRAY(4) = DINC = DISTANCE I	
5000 DOE+01	ARRAY(5) = NSTART = INDEX OF	THE FIRST DISTANCE AT
1000° 10E+01	ARRAY(6) = NZINC = THE FIELD DISTANCE ARRA	IS TO BE FOUND AS A Y NZINC MUST NEVER BE
3370103E+03	ARRAY(7) = INDEX OF THE LAST	DISTANCE AT WHICH THE
3000100F+04	ARRAY(8) = 7MIN = THE MINIMU	M ALTITUDE ABOVE THE
1000000E+02	ARRAY(9) = 7INC = THE ALTITU	DE INCREMENT, METERS
3 (000 005+04	ARRAY(10) = ZMAX = THE MAXIM	SETEM . SCUTITUA MU
1000 OnE+04	APRAY(11) = FLAT = THE FACTO	R USED IN THE FLAT EARTH
850000E+00	APPAY(12) = ALPHA = VERTICAL	LAPSE FACTOR
74919 47E+07	ARPAY(13) = EFFECTIVE EARTHS	RADIUS
10000 00E+01	ARRAY(14) = NUT	
ENAM1		
TOA = .45.0	767079568845+03, .1163720838536	55=+64, .111319579318393
TD1 = . 172	4C37375896*E+15.	
TD2 = .26 A	165387176155+15.	
501 = -125	37425+25,	
ED2 = .251		

DISTOUM = .12781571845427+37, .748706681238215+03, .337302533188285+33, ...

IIMDUM = .16250234178697+01, .167124931832597+71, .142135133147947+01, ...

DISTON = .1779122027422776+03, .348285440253896+07, .333193665501727+13,

IPW = .459848105575185+13, .116214362610965+04, .114479179217.35+14,

4. DESCRIPTION OF PART II

4.1 Overview

The electrical properties of the earth are converted into a ground surface impedance in PART II of the program as shown in Figure 7. The data on the input tapes from PART I are loaded on to a disc so that at each index point information on terrain, geology, and soil is available. This information is employed to develop a 3-layer model of the ground as shown in Figure 8. The time of arrival of the LORAN pulse at the receiver is controlled by the electrical characteristics of this model through a parameter called the surface impedance. This parameter is the ratio of the horizontal components of the electrical to the magnetic field components assuming the ground is isotropic; the calculation of this parameter is described by Johler. 12, 13

The development of the 3-layer ground model requires additional investigation, in particular, the constants to be used in the postulated second or saturated layer. The electrical characteristics of ground or other medium may be expressed by three constants, the relative permeability, the dielectric constant, and the conductivity. The relative permeability can normally be regarded as unity. From the digitized data from PART I, the conductivity of the top unsaturated ground or soil and basement rock can be determined. 14, 15, 16, 17, 18 Most soil maps also contain information on top soil depth which is included in the look-up table. The rock depth is assumed to be infinite since the 100 kHz wave does not penetrate below 300 meters. The conductivity and depth of the second layer are somewhat uncertain and various articles in the journal titled Geoexploration 19, 20 have been used to obtain information on second layer parameters as a function of the top layer. The values listed in Figure 8 are suitable for Europe. In Iran, for example, sigma 2 is larger than sigma 1. The dielectric constant has been selected as 15 over land and 80 over water. An empirical relationship between conductivity and dielectric constant has been developed by Hanle. 21 and may also be used in the

Due to the large number of references on this page, the references will not be footnoted. See References, page 84.

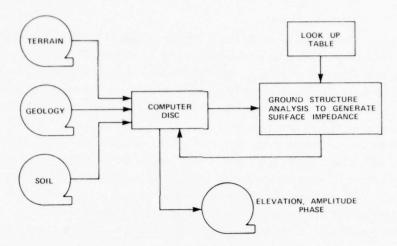


Figure 7. Data Base of Ground Electrical Properties - Part II

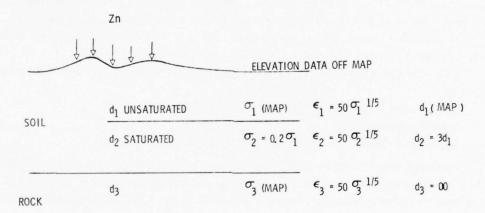


Figure 8. Ground Model for Surface Impedance Calculators

program. The effects of temperature changes, vegetation, buildings, and other objects on the surface of the earth have not been considered.

The input data to PART II is on a standard one-half inch, 400-foot magnetic tape containing information on elevation in meters, bedrock, and soil identification number. The input format for the data is as follows:

Elevation - 11 bits - ±7 meters

Blank - 3 bits

Rock Number - 8 bits - 256 types

Blank - 2 bits

Soil Number - 6 bits - 64 types

This totals to a 30-bit data word. Each CDC word contains 60 bits, therefore, two data words or points can be accommodated by a single CDC word. For 30-bit word computers (IBM 360, UNIVAC, Honeywell), one data point will be accommodated by each word allowing flexibility between machines. There are 60 words in each record or $2 \times 60 = 120$ data points. With a 30 arc second grid, each record covers one degree in latitude of the grid.

The data is recorded on to the tape in the following sequence: Starting at 6° E Long, 48° N Lat, in the southwest corner and go north for one degree in latitude (one record), then repeat for an equal line incremented in longitude, parallel and 30 arc seconds to the east of the first line. This is repeated until the last longitude line of the two degree standard longitude sectors is reached. For this particular problem, this would mean after $2 \times 60 \times 2 = 240$ records. The latitude is then incremented by one degree, returned to the original longitude, and the entire process repeated for another 240 records. At the east edge of the final latitude sector $(53^{\circ}$ to 54°), the pointer returns to 8° N Lat and begins another 1° latitude scan from 8° E to 10° E longitude. For the six degree latitude and eight degree longitude area coverage in Germany, there will be a total of $960 \times 6 = 5760$ records which contain $5760 \times 120 = 691$, 200 data points.

The output data tape of PART II which is the input to PART III has the following format:

Elevation in meters $-\pm 7$ meters -11 bits Impedance Amplitude $-\pm 2$ ohms -8 bits Impedance Phase $-\pm .001$ radians -11 bits

The elevation data is passed directly from input to output tape. The output impedance is returned to the disc for storage in the same location as the original data and then recorded on magnetic tape for shipment to the PART III computation sites.

4.2 Subroutine Description

4.2.1 PROGRAM CONIMP

- (a) Controls impedance program.
- (b) Call subroutine SETUP.
- (c) Reads and writes on disc soil, geology and elevation identification data off input tapes.
 - (d) Call subroutine REPK.
 - (e) Writes impedance data on disc and output tape.

4.2.2 SUBROUTINE SETUP

- (a) Sets relative permeability of three layers to unity.
- (b) Reads and stores ground conductivity tables from input cards into look-up file.

4.2.3 SUBROUTINE REPK

- (a) Determine parameters for 3-layer ground surface impedance.
 - (1) Dielectric constant equals fifteen overland and eightly over
 - (2) Determine depth of first and second layer. Set third layer to infinity.
 - (3) Set sigma 2 as a function of sigma 1.
- (b) Call subroutine GRIM for impedance calculation.

4.2.4 SUBROUTINE GRIM

- (a) Calculates surface impedance for 3-layer ground model.
- (b) Returns complex impedance (AMP, FAZ) to subroutine RFPK via argument list.

4.3 Resistivity Tables

For subroutine SETUP, a look-up table is required to convert type of soil and rock into resistivity values. The bibliography at the end of this section lists available sources for these values. Table 1 is a list of average values for the top or unsaturated soil. An approximate value is usually assigned in the map legend.

An inspection of the geological map of Europe reveals characteristic rock types which include anorthosite, granite gneiss, gabbro, Precambrian igneous, and metamorphic rock. The associated resistivities for various rock types are defined in Table 2.

Table 1. Ground Resistivity Values for Typical Soils

Terrain	Conductivity (mhos-meter)	Resistivity (meter-ohms)
Sea water	5	0.2
Fresh water	8 × 10 ⁻³	123
Dry, sandy, flat coastal land	2×10^{-3}	300
Marshy, forested flat land	8 × 10 ⁻³	123
Rich agricultural land, low hills	1 × 10 ⁻²	1,00,0
Pastoral land, medium hills and forestation	5 × 10 ⁻³	200
Rocky land, steep hills	2×10^{-3}	500
Mountainous	1 × 10 ⁻³	1,000
Cities, residential areas	2×10^{-3}	500
Cities, industrial areas	1 × 10 ⁻⁴	1,0000

Table 2. Rock Types and Resistivities

Effective Resistivity Meter-ohms	min max mean	1,000 14,000	200	400 7,000 1,500	1,000 5,000 2,200	a 1,000 2,000 1,800	65 180 140	50 140 100	150 480 300	55 70 65	170 380 200	20
Secondary	Rock Types		Alluvium	Slate	Sandstone	Quartzite & Limestone	Limestone	Limestone & Shale	Limestone		Limestone Shale	Shale
Principle	Rock Type	Granities, etc.	Gneisses, Granites, etc.	Gneisses, Granites, etc.	Gneisses, Granities, etc.	Granites, etc.	Gneisses, Granites, etc.	Sandstone	Sandstone	Shale	Sandstone	Limestone
Secondary	Geologic Age			Cambrian	Cambrian	Cambrian & Ordovician	Cambrian & Ordovician	Ordovician	Ordovician Silurian Carboniferous		Silurian Devonian	Silurian
Principle	Geologic Age	Precambrian	Precambrian	Precambrian	Precambrian	Precambrian	Precambrian	Cambrian	Cambrian	Ordovician	Ordovician	Ordovician

Table 2. Rock Types and Resistivities (Cont.)

Drinciple	Secondary	Principle	Secondary	Effec	Effective Resistivity	vity
Geologic Age	Geologic Age	Rock Type	Rock Types	min	max	mean
Ordovician	Carboniferous	Sandstone	Limestone & Shale	62	06	75
Cambrian	Ordovician	Sandstone	Limestone, Shale, Alluvium			9
Cambrian	Ordovician	Limestone	Shale	170	300	200,
Cambrian	Ordovician Silurian	Sandstone	Limestone & Shale	38	180	130
Cambrian	Ordovician Carboniferous	Sandstone	Limestone & Shale	250	310	280
Cambrian	Ordovician Silurian Carboniferous	Sandstone	Limestone & Shale	350	909	480
Ordovician	Silurian, Devonian & Carboniferous	Sandstone	Limestone & Shale	71	105	100
Ordovician	Triassic	Sandstone	Limestone & Shale	170	270	205
Silurian	Devonian	Limestone		55	02	62
Silurian	Devonian	Limestone		62	84	72
Silurian	Devonian	Sandstone	Limestone & Shale	290	440	350
Devonian		Sandstone	Shale	200	400	290

Table 2. Rock Types and Resistivities (Cont.)

Principle	Secondary	Principle	Secondary	Effec	Effective Resistivity Meter-ohms	vity
Geologic Age	Geologic Age	Rock Type	Rock Types	min	max	mean
Devonian	Carboniferous	Sandstone	Shale	19	34	29
Carboniferous		Sandstone	Shale			20
Carboniferous		Sandstone	Shale			10
Carboniferous		Sandstone	Limestone & Shale	20	40	25
Carboniferous		Limestone	Alluvium			28
Carboniferous		Limestone				2
Carboniferous	Triassic	Sandstone	Limestone	40	44	40
Carboniferous	Cretaceous Tertiary	Sand	Clay Loam			40
Carboniferous	Cretaceous Tertiary	Marl	Sand Clay	22	26	25
Carboniferous	Quarternary	Sand	Shale Alluvium	œ	11	10
Triassic		Sandstone	Shale, Trap & Diobase	150	350	250
Cretaceous		Chalk				5.4
Cretaceous		Sandstone	Clay	10	15	13
Cretaceous	Tertiary	Sand	Clay	13	17	17

Table 2. Rock Types and Resistivities (Cont.)

rity	mean	∞	10	31	9	9	15	19	ro
Effective Resistivity Meter-ohms	max				7	9		20	80
Effec]	min				4.5	5.5		18	4
Secondary	Rock Types	Clay	Sand Clay	Clay	Clay	Clay	Clay	Clay	Clay
Principle	Rock Type	Sand	Marl	Sand	Sand	Sand	Sand	Sand	Sand
Secondary	Geologic Age	Tertiary Quarternary	Tertiary Quarternary				Quarternary	Quarternary	
Principle	Geologic Age	Cretaceous	Cretaceous	Tertiary	Tertiary	Tertiary	Tertiary	Tertiary	Quarternary

4.4 Program Listing for Part II

PROGRAM CONIMP

1		PROGRAM CONIMP(TAPE3, TAPE2, INPUT=128, OUTPUT=128)
-		COMMON/THREE/F, PHI, SIGMA1, E21, AMU1, Z1, SIGMA2, E22, AMU2, Z2, SIG MA3,
		E23,AMU3
		COMMON/CODE/SLCO(65,3),G0,GLCO(148)
5		DIMENSION NUPK(60), NDXEQ(5800)
		DATA MSK6/778/, MSKF15/77777000000000000000000000
		LNLM=960\$LATLM=6
		LNLM=2C\$LATLM=1
		NDXSIZ=LNLM*LATLM+40
10_		CALL SETUP
		CALL OPENMS(2, NDXE0,5800,0)
		L NL M= 5760
		DO 100 ILN=1,LNLM
		NDXL=ILN
15		BUFFERIN(3,1) (NUPK(1), NUPK(60)) \$ IF (UNIT(3)) 10,20,30
		PRINT1, ILN
	_	FORMAT(*0 PARITY ERROR*,19)
	10	CONTINUE
		IF(MOD(ILN,1440).LT.10)PRINT 9, ILN, NDXL, NUPK (1), NUPK (2)
20		CALL REPK (NUPK, MSK6, MSKF 15)
		IF(MOD(ILN,1440).LT.10) PRINT 99, NUPK(1), NUPK(2)
		IOVER=1
		IOVER=0
		CALL WRITMS(2, NUPK, 60, NDXL, IOVER)
25		FORMAT(*0 *,218,2022)
_		FORMAT(2022)
		CONTINUE
	20	STOP\$END

SUB ROUTINE REPK

1	SUBROUTINE REPK (NUPK, MSK6, MSKF15)
	COMMON/THREE/F, PHI, SIGMA1, E21, AMU1, Z1, SIGMA2, E22, AMU2, Z2, SIG MA3
	.E23,AMU3
	COMMON/CODE/SLCD(65,3),G0,GLCD(148)
5	DIMENSION NUPK(60), IAB(120)
	DATA MS K8/3778/
	MSK30=37770000003777000000B
	DO 100 I=1,60
	LLEV=NUPK(I).A.MSK30\$LEV=SHIFT(LLEV,1)
10	LS2=NUPK(I).A.MSK6\$LG2=MSK8.A.SHIFT(NUPK(I),-6)
	LS1=MSK6.A.SHIFT(NUFK(I),-3C)\$LG1=MSK8.A.SHIFT(NUPK(I),-36)
	DO 99 I2=1,2\$IF(I2.EQ.2)LS1=LS2\$IF(I2.EQ.2)LG1=LG2
	E23=E22=E21=15.
	IF(LS1.EQ.0.OR.LS1.EQ.22.OR.LS1.EQ.12.OR.LG1.GE.146) E22=E21=80.
15	SIGMA1=SLCD(LS1+1,1)
	71=SLCD(LS1+1,2)*0.75
	IF(Z1.LT.2.) Z1=2.
	IF(Z1.LT.SLCO(LS1+1,3))Z1=SLCO(LS1+1,3)
	IF(SIGMA1.EQ01)E22=E21=80.

20	SIGMA 2= 0. 5*SIGMA1 \$Z2=4.* Z1	
	IF (E22.EQ.87.)SIGMA2=SIGMA1	
	ILAT= 2* T+ I2-2	
	SIGMA 3= GLCD(LG1) \$ CALLGRIM (AMP, FAZ) \$ IA MP=A MP\$ IFA Z=FAZ	
	NR=30*(2-I2)	
25	99 LEV=OR(SHIFT (IAMP, NB+11), SHIFT (IFAZ, NB), LEV) \$NUPK(I) = LEV	
	100 CONTINUESEND	

SUBROUTINE GRIM

1	SUBROUTINE GRIM (AMPIMF, FAZIMP)
	CF IS FREQUENCY IN HEPTZ
	CPHI IS THE ANGLE OF INCIDENCE IN RADIANS
	CSIGMA1 IS THE CONDUCTIVITY OF THE UNSATURATED SOIL.
5	CE21 IS THE DIELECTRIC CONSTANT OF UNSATURATED SOIL.
	C71 IS THE DEPTH IN METERS OF THE UNSATURATED SOIL)
	CSIGMA2 IS THE CONDUCTIVITY OF THE SATURATED SOIL.
	CE22 IS THE DIELECTRIC CONSTANT OF SATURATED SOIL.
	CZZ IS THE DEPTH IN METERS OF THE SATURATED SOIL.
10	CSIGMA3 IS THE CONDUCTIVITY OF REDROCK.
-	CE23 IS THE DIELECTRIC CONSTANT OF BEDROCK.
	CZSOIL IS THE TOTAL DEPTH OF SOIL ABOVE REDRCCK (Z1 + Z2)
	COMPLEX T2N, T20
	COMPLEX A10, A20, A11, A12, A13, A21, A22, A23, A32, A33,
15	1 A 3 4 , A 4 2 , A 4 3 , A 4 4 , A K1 , A K2 , ETA 1 , ETA 2 , ETA 1 2 , ETA 2 2 ,
	ZZETA1, ZETA12, ZETA2, ZETA22, TEMP, RENUM, REDEM, RE. PMI.BETA1
	COMPLEX SAV1, SAV2, SAV3, SAV4, SAV5, SAV6
	COMPLEX AK3, FTA3, ETA32, ZETA3, ZER01, A54, A55, A64,
	1A65, A66, T2, T3N, T3D, T3 , A35, A45, A56
20.	COMMON /THREE/ F , PHI , SIGMA1, E21, AMU1, Z1, SIGMA2,
20	1E22, AMU2, Z2, SIGMA3, E23, AMU3
	DATA (C = 2.997925F8), (TPI=6.2831853071796)
	DATA(ED = 8.8541853367321E-12)
	DATA(PI = 3.141592654) , (PI2 = -1.570796327)
25	DATA ISKIP/1/
25	IF(ISKIP.EQ.O)GO TO 99
	ISKIP = 0
	ZER01 = CMPLX (0.,1.)
	1 COSPHI = COS (PHI)
70	SINPHI = SIN(PHI)
30	COSS = COSPHI * COSPHI
	SIN2 = SINPHI * SINPHI
	OMEGA = F * TPI
	ETA0=1.000338
35	AKD=OMEGA/C*ETAD
	OMEGAE = OMEGA * EO
	EPSIL=1.E-15
	10 A10 = CMPLX(-COSPHI, 0.)
	A11 = A10
40	A12 = A13 = A20 = A34 = A35 = CMPLX(-1.,0.)
	A56 = CMPLX(1.,0.)
	A21 = CMPLX (1., n.)
	99 AK2=AK0 +CSORT (CMPLX(E22, -SIGMA2/OMEGAE))
	ETA2 = AK2/AK0

```
45
           ETA22 = ETA2 * ETA2
           TEMP = ETA22 - SIN2
           ZETA2 = CSORT (TEMP)
           A44 = 7ETA2 *( SIN2 / (AMU2 * ETA22-SIN2) + 1.) /AMU2
           A45 = -444
           AK3 = AK0 * CSQRT (CMPLX(E23, -SIGMA3/OMEGAE))
50
           ETA3 = AK3 / AKO
           ETA32 = ETA3 + ETA3
TEMP = ETA32 - SIN2
           ZETA3 = CSORT (TEMP)
           A66 = ZETA3 * (SIN2 / (AMU3 * ETA32 -SIN2) + 1.) / AMU3
55
           CONTINUE
           AK1 = AK0 *CSQRT( CMPLX (E21, -SIGMA1/ OMEGAE))
        20 ETA1 = AK1/AK0
           ETA12 = ETA1 * ETA1
TEMP = ETA12 - SIN2
60
           ZETA1 = CSORT (TEMP)
           A22 = A23 = -ZETA1 *(SIN2/ (AMU1 * ETA12-SIN2 ) +1.) /AMU1
           A23 = -A23
           BETA1 = AKO * ZETA1 * Z1*ZERO1
        30 A32 = CEXP(-BETA1)
65
           A33 = CEXP (RETA1)
           A42 = A22 * A32
A43 = A23 * A33
           BETA1 = AKO * ZETA2 * ZZ * ZERO1
70
           A54 = CEXP (-BETA1)
           A55 = CEXP (BETA1)
A64 = A44 * A54
           A65 = A45 + A55
           T2N=A54 *A66-A64 *A56
           T 20= 455 * 466 - 465 * 456
75
           A1=A2=A3=A4=A9S(SIGMA2-SIGMA3)
           IF(((A1.LT.EPSIL ).AND.(A2.LT.EPSIL )).OR.
          1 ((A3.LT.EPSIL ).AND. (A4.LT.EPSIL )))GO TO 31
           T 2=T 2N/T2D
           GO TO 32
80
        31 CONTINUE
           T 2= 0.
        32 CONTINUE
           T3N = (A32 * A44 - A42 * A34) - (A32 * A45 - A42 * A35) * T2
T3D = (A33 * A44 - A43 * A34) - (A33 * A45 - A43 * A35) * T2
85
           A2 = A4 = ABS(SIG MA2 - SIGMA3)
           A1=A3=ABS(SIGMA1-SIGMA2)
           IF (((A1.LT.EPSIL ).AND.(A2.LT.EPSIL )).OR.
          1((A3.LT.EPSIL ).AND.(A4.LT.EPSIL )))GO TO 34
           IF (A1.LT.EPSIL) T3=T2*A32/A33
90
           IF(A1.GE.EPSIL)GO TO 36
           B1=REAL (T2)
           B2 = AIMAG(T2)
           B3=REAL (T3)
95
           B4=AIMAG(T3)
      115 FORMAT(* *,8 (E13.5,2X))
        36 CONTINUE
           IF( A1.LT.EPS IL) GO TO 35
           T3 = T3N / T3D
           GO TO 35
100
        34 CONTINUE
           T3=0.
        35 CONTINUE
           RENUM = (A10 * A22 - A20 * A12) - (A10 * A23 -A20 * A13) * T3
```

```
REDEM = (411 * A22 - A21 * A12) - (A11 * A23 - A21 * A13 ) * T3

RE = RENUM / REDEM
TEMP = (1. - RE) / (1. + RE)
PMI = TEMP * COSPHI
50 AMPIMP = CABS(PMI)

110 FAZIMP = CANG (PMI)
IF (FAZIMP.LE.PI2) FAZIMP = FAZIMP * PI

IF (FAZIMP.LE.PI2) FAZIMP = FAZIMP - PI
IF (FAZIMP.LT.J.O.050) FAZIMP=0.050$IF (FAZIMP.GT.1.400) FAZIMP=1.400
IF (AMPIMP.LT.O.001) AMPIMP=0.001$IF (AMPIMP.GT.O.200) AMPIMP=0.200

115 AMPIMP=1000.*AMPIMP$FAZIMP=1000.*FAZIMP
IF (FAZIMP.LT.O..OR.AMPIMP.LT.J.) PRINT 1776

1776 FORMAT(*O AMP OR PHASE NEGATIVE*)
RETURN
FNO
```

FUNCTION CANG

1	FUNCTION CANG(Z)
	C
	C
	COMPLEX Z
5	C
	<u>C</u>
	C
	CINITIALIZE CANG FOR QUADRANT CORRECTION, GET RE(Z) AND IM(Z), TES
	CX FOR + OR - TO FIND CORRECT HALF-PLANE
10	DATA (C = 2.997925E8), (TPI=6.2831853071796)
	PI2 = TPI
	PI = TPI /2.
	PIO2 = TPI / 4
	CANG=0.0
15	X=REAL(Z)
	Y = A I M AG(Z)
	IF (X) 10,50,90
	CX .LT. 0.0
	10 IF (Y) 20,30,40
20	20 CANG=-PI
	GO TO 90
	30 CANG=+PI
	RETURN
	40 CANG=+PI
25	GO TO 90
	CX .EO. 0.0
	50 IF (Y) 60,70,80
	60 CANG=-P IO 2
	RETURN
30	CX=O AND Y=O IS REALLY UNDEFINED, BUT IN AGREEMENT WITH CDC WE
	C RETURN A VALUE OF CANG=0.0
	70 CANG=0.0
	RETURN
	80 CANG=+PIO2
35	CX .GT. 0.0 AND X .6T. 0.3 ADJUSTED FOR CORRECT QUADRANT
	90 CANG=ATAN (Y/X) + CANG
	RETURN
	END

SUBROUTINE SETUP

1	SUBROUTINE SETUP
	COMMON/THREE/F, PHI, SIGMA1, E21, AMU1, Z1, SIGMA2, E22, AMU2, Z2, SIGMA3
	• E 23, AMU3
	COMMON/CODE/SLCD(65, 3), 60, GLCD(148)
5	DATA CFW/1.E-2/,CSW/5./,CWG/1.E-2/,CDG/1.E-4/
	TPI=8.*ATAN(1.0)\$F=1.E5\$PHI=80.*(TPI/360.)
	A HU 1= AHU?= AHU3=1.
	00 1 I=2,65
	1 READ 16, SLCD(I,1), SLCD(I,3), SLCD(I,2)
18	13 FORMAT(10X,F10.1,F10.1,F10.1)
	$002I = 1,19\$I9 = (I-1)*8+1\$IE = IB+7\$IF(I_0EQ_019)$ IE = 148
	2 READ11, (GLCD(K), K=IB, IE)
	11 FORMAT(8F10.1)
	00 3 I=2,65
15	PRINT5, I, SLCD(I, 1), SLCD(I, 2)
	3 SLCD(I,1)=1./SLCD(I,1)
	5 FORMAT(15,2F15.1)
	PRINT 6\$D04I=1,148\$PRINT5, I,GLCD(I)
	4 GLCD(I) =1./GLCD(I)
20	6 FORMAT(*0 GEOLOGY RESISTIVITY*,//)
	GLCD(0) = SLCD(1,1) = CFW\$SLCD(1,2) = 20.
	SLCD(1,3)=20.
	SLCD(65,1)=CFH\$SLCD(65,2)=20.
	SLCD(65,3)=20.
25	E ND

5. DESCRIPTION OF PART I

5.1 Overview

The lithology and terrain of the LORAN coverage area are digitized from maps in PART I as illustrated in Figure 9. The required three maps are those which contain information on the type top soil or overburden, type or age of basement rock, and ground elevation above sea level. The first type of information is obtained from soil maps usually published by the country of the interested area. These are colored maps with a legend defining the various types of soil and associated depth. Geological maps are available for most areas of the world and the colored legend indicates the type of rock. Terrain maps with elevation data are readily available for the entire world. Fortunately, these have been previously digitized by the Defense Mapping Agency, and magnetic tapes with this data in proper sequence are available upon official request.

The following equipment was required for data digitization:

Calculator - HP9830A

Digitizer - HP9864A

Cassette Memory - HP9865A

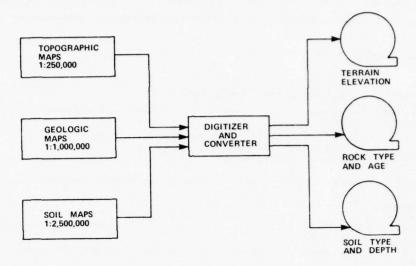


Figure 9. Formation of Data Base - Part I

The maps are digitized by recording, on a cassette tape, the contour table coordinates in inches using the southwest corner as the origin. The cursor cross hairs are moved around each constant color contour and points are generated in increments of one hundred to the inch. The table coordinates and geographic coordinates of the four corner points of the map are recorded for later use in conversion of the former to the latter. These cassette tapes are transcribed onto a disc file by way of the CDC 6600. The merged cassette data is then copied on to a 1/2-in. 2400-ft 800-bpi tape reel. The data on this tape is converted to LAT/LON and color number, and then into scan lines by PROGRAM GGCI. The scan line output format contains 24 bits for longitude, 24 bits for latitude, and 12 bits for color, making up the 60 bit CDC word. These points will then be sorted in PROGRAM SOR with the primary key being the latitude, secondary key the longitude, and tertiary key the color. PROGRAM DECODE sequences the sorted line points into a 30 arc second matrix for the final output tape of PART I. These programs are listed in Section B. Three such magnetic tapes are required, one for each of the ground properties. For a coverage area of 48 square degrees, there will be almost 700,000 data points recorded on each 7-track binary magnetic tape.

The Defense Mapping Agency generates similar data tapes in a program titled "Lineal Data to Terrain Matrix." This program is capable of forming a data matrix from map contour scans with a three arc second to a one minute spacing. By using the standard DMA format as input specification to PART II of the prediction program, DMA and locally generated tapes can be used interchangeably. The

present program is setup for a thirty arc second grid. Changes in this spacing will require changes in the incremental sequencing and storage allocations.

5.2 Program Listing for Part I

	PROGRAM SOR (TAPE3, TAPE2, TAPE4, TAPE1) 9 READ(1) IP
	TEGOT (1); 2,1 WRITE(2) IP\$GO TO 9 CONTINUETREWIND 2\$CALL SMSOPT(10) CALLSMFILE("SORT", "BINARY", 2, "REWIND") CALL SMFILE("OUTPUT", "BINARY", 3, "REWIND") CALL SMKEY(1,1,10,0," INTEGER") CALL SMKEY(1,1,10,0," INTEGER")
	2 CONTINUE TRENING 2 CALL SMSORT (10)
	CALLSMFILE("SORT","BINARY",2,"REWIND")
	CALL SMETCH (1.10.0 "INTEGER")
	REWIND 3 5 READ(3) IP
	ÎF (E)F (3)) 4, 3
	IF(E)F(3))4,3 3 WRITE(4)IP GO TO 5
	4 STOP\$FND
MC 60	21150,CM77777,TP2. 2096 M-CONISH
VSN.	TAPE1=0S 0139.
RECU	EST, TAPE 1, HY, L, NR. TAPE 2= OS 0172. EST, TAPE 2, HY, L, RING. (TAPE 2, R T= S, BT= G)
VSN,	TAPE 2 = 05 01 72 •
FILE	(TAPE 2, RT=S, BT=C)
LUSE	T(FILES=TAPE2)
Feo.	PROGRAM DECODE (INPUT.OUIPUT.TAPE6=OUIPUT.TAPE5=INPUT.TAPE1.TAPE2)
	PROGRAM DECODE(INPUT, DUTPUT, TAPE6=OUTPUT, TAPE5=INPUT, TAPE1, TAPE2) COMMON IOUT(721), ICURPT, IMINH, IMAXH, IMINH2, IMAXH2, INFLOO
	DIMENSION Y(5001), 1C(5001), 1RÚF (512) DIMENSION MONE(721), MTHO(721), MSAVE(721)
	ISTOP= 0 XXDE3 = 6.
	AASE=1
	D0 11
11	IOUT (I 6) = 0 120=513
	120=513 LEN=512
	ĪĪOT=0
	XCUR = 0 . XCNT = X XDEG
	XCNT=XXDEG IMINH= 0
	ĪMĀXH= 0
	TMINH2 == 1000 IMAXH2 == 1000
	199H1= -1000
	<u>199H1=-1009</u> <u>199H2=-2000</u>
C SK	IEZ=0 IP TEST DATA
-0-01	IPHASE = 1
15	CONTINUE
	J=1 TPHASE=2
	ĬE=0 ĪFIRST=1
	IL IK21 = I
4	CONTINUE
C 4	INFLOO = 0 IS TO READ IN ANOTHER SCAN LINE
•	IS TO READ IN ANOTHER SCAN LINE IF(IFIRST EQ.1) GOTO6
	IF (XCUR.LT. (XXDEG004)) GO TO 6
_	
Č	** -DECODE MODIFICATIONS (START) ** -MODIFICATIONS (BRUCE HAINES 8/18/76)
U	HOUTE TOWN TOWNER HAINES 0/10/10/

```
8005 KA=1,721

8005 MSAVE(KA)=IOUT(KA)

IF(MCASE.GT.1) GO TO 8010

8007 MONE(KA)=IOUT(KA)

GO TO 8400

8010 IF (MCASE.GT.2) GO TO 8030

00 8015 KA=1,721

8015 MTHO((A)=IOUT(KA)

GO TO 8250
  C
                                                           ** -FOR NORPAL SCANS
8030 DO 8100 KA=1,721
IF (MTWO(KA).EO.0) GO TO 8050
IOUT(KA)=MTWO(KA)

8050 IF (IOUT(KA).EQ.0) GO TO 8070
GO TO 8100
8070 IF (MONE(KA).EQ.0) GO TO 8080
IOUT(KA)=MONE(KA)

8080 IF (KA.EQ.1) GO TO 8100
IOUT(KA)=IOUT(KA-1)
8100 CONTINUE
     8100 CONTINUE

DO 8105 KA=1,721

MONE (KA) = MTW C (KA)

HTWO (KA) = MSA VE (KA)

8105 CONTINUE

GO TO 8300
                                                           ** -FOR LAST SCAN LINE ONLY
    C
    8170 00 8200 KA=1,721
IF (MTWO(KA).EQ.0) GO TO 8180
IOUT (KA)=MTW (KA)
GO TO 8200
8180 IF (MONE(KA).EQ.0) GO TO 8190
IOUT (KA)=MONE(KA)
GO TO 8200
8190 IF (KA.EQ.1) GO TO 8200
IOUT (KA)=IOUT (KA-1)
8200 CONTINUE
ISTOP=1
GO TO 8300
C
  C
    C
                                                           ** -FOR FIRST SCAN LINE ONLY
8250 DO 8270 KA=1,721

IF(MONE(KA).EO.0) GO TO 8255

IOUT(KA)=MONE(KA)

8255 IF(MIHO(KA).EQ.0) GO TO 8260

IOUT(KA)=MTHO(KA)

GO TO 8270

8260 IF(KA.EQ.1) GO TO 8270

IOUT(KA)=IOUT(KA-1)

8270 CONTINUE
   ** -DECODE MODIFICATIONS ... (FINISH)
```

```
6
  9
  7
  603
   2
C READ IN A POINT.
31 CONTINUE
READ(1) IP
                 IF (EOF (1)) 50,1
  1 XNEW=FLOAT(SHIFT(IP,-36))/120.

IF (XNEW.LT.XCUR) GOTO31

Y(I3)=FLOAT(SHIFT(IP,-12).ANO. 7777 7777 B)*.001

IC(I3)=IP.AND. 7777 B

IF(IC(I3).GT.300) GOTO 220

C FOR GLITCHES
                GLITCHES

IF ((XNEW.LT.5).0R.(XNEW.GT.15)) GOTO 221

IF ((Y(I3).LT.47) .OR. (Y(I3).GT.55)) GOTO 221

IF (J.EQ.1.AND.I3.EQ.1) XCUR=XNEW

IF (XCJR.NE.XNEW) GOTO 3

IF (I3.EQ.1) GOTO 10

IF (Y(I3).LT. Y(I3-1)) GOTO 302

CONTINUE
PRINT 604

FORMAT(* ERROR AT 604*)

STOP

PRINT*.** SIMI NO. 98 ENCOUNTERED. FINISHED."
32
  10
604
                 PRINT ," STMT NO. 98 ENCOUNTERED. FINISHED."
98
                 STOP
PRINT*," IC.GT.300, PROBABLE GLITCHES."
GOTO 31
WRITE(6,2601)
FORMAT(" COORDINATES OUT OF RANGE. PROBABLE GLITCHES.")
   220
   221 2601
                 GOTO 31
WRITE(6,3601)
FORMAT (6 (" A POINT OUT OF ORDER"))
Y(13)=Y(13-1)
GOTO 10
  302
3601
  C INITIALIZATION FOR PROCESSING

CONTINUE
PRINT*, "END OF DATA. ITOT=",ITOT
IE=1
C IE=END OF FILE SWITCH
GOTO1
 162=1
3 CONTINUE
IFIRST=0
L=I3-1
C GO FROM 1 TO L WITH ARRAYS
YSAVE=IC(I3)
ICSAVE=IC(I3)
Y(I3)=0
IC(I3)=0
J=2
  49
                 IE2=1
J=2
IF(XCJR.LT.(XXDEG-.004)) GO TO 4
C PRINT SCAN LINE
```

```
C BEGIN PROCESSING (FLOHCHART)
C ICURPT IS CURRENT POINT
ISP1=0
  45
               CONTINUE
CONTINUE
ICURPI = ICURPI+1
IF (ICURPI) GOTO 80
   79
               IF(ICURCL.NE.IC(ICURP))) 6010 80

601081

CONTINUE

IF((199H1.E0.I99H2).AND.(199H2.EQ.ICURPT)) G0TO 105

I99H1=199H2

I99H2=ICURPT

IF (ISP1.NF.D) G0TO 83

ICURPT = ICURPT-1

ICURCL = IC(ICURPT)
80
   106
                GOT 025
ISP1=ISP1+1
GOTO 106
ICURPT=ISP1
105
   83
               GOVER = 1501

GOVER = 1502

GOT 025

CALL FILL (Y(ICURPT-2),Y(ICURPT),IC(ICURPT))

ICURCL = 1501

GOT 025
81
   C
72
  72 CONTINUE
C HOLE SSSUMED(CASE1)
74 CONTINUE
IF (ICURPT.GE.L) GOTO4
C IS THIS END OF SCAN LINE
C 4 IS TO READ IN ANOTHER SCAN LINE
ICURPI=ICURPI+1
ISP1=ICURPI-1
CALL FILL(Y(ICUPPI-1),Y(ICURPI),IC(ICURPI))
C IF NOT WITHIN 015, GO TO 72
ICURPI=ICURPI+1
ISC2=IC(ICURPI)
                CONTINUE
```

```
C (IN CASE BACKWARDS)
ICURCL=IC(ICURPT)
GOT 0 25
END
GOTO 25
END
SUBROUTINE FILL (YMIN,YMAX,IC)

C FILLING IN COLOR NUMBERS
COMMON IOUT(721), IGURPT, IMINH, IMAXH, IMINH2, IMAXH2, INFLOO

INFLOO = INFLOO+1

IF (YMIN,LT,48,) YMIN=48,

IF (YMAX,LT,48,) YMIN=54,

IF (YMIN,GT,54,) YMIN=54,

IF (YMIN,GT,4NAX) GOTO:

IARYMIN = (YMIN-48,) *120,*1.*.5

CITIS ASSUMED THAIT THE REAL VALUE HILL BE TRUNCATED

IF ((IARYMIN,EQ,IMINH),AND,(IMAXH,EQ,IMAXH)) GOTO 3D

IMINH=IMINH
IMAXH=IMINH
IMAXH=IMINH
IMAXH=IMINH
IMAXH=IARYMAX
C FILL UP AN ARRAY OF LENGTH 721

DO 1001 I=IARYMIN,IARYMAX
IOUT(I)=IC

CONTINUE
RETURN
1 PRINTS1
51 FORMAT(* ABORTED BECAUSE SUBROUTINE WAS CALLED WITH YMINIYMAX*)
STOP
30 ICURPT=ICURPT+3
CO TO 31$END
MC64,1450,CM255000,TP2,
FIN(SL,PL=99999)
VSN,TAPE1=GGC64C.
REQUEST,TAPE1,HY,L,RING.
SKIP.
  LGO.
SKIP.
```

```
994 FORMAT (* INCORRECT SLOPE COMPUTATION *)
PHIR1=48.0 $ PHIR6=50.0 $ PHIR11=52.0 $ PHIR16=54.0
READ 1,NUMBEC
PRINT 2,NUMBEC
PRINT 2,NUMBEC
NOTE 1
100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NOTE 1 100 NO
                                                                NT=0
PRINT 135, IAGE, NOFTREC
IF (NOFTREC.GI.6) PRINT 944
G0 T0 100
IF (IBL KNO.EQ.1) 141, 142
NDXLAT(1) = IXST $ NOYLONG(1) = IYST
PRINT 145, IXST, IYST, NUMVEC, ISTVEC
N=NUMVEC
              140
141
142
        C
                                                                    NDYLONG(J+1) = NOYLONG(J)
```

```
600 CONTINUE
                                    NT=NT+NUMVEC

IF (IBLKNO.LT.NOFTREC) 100,602

NOVEC(IAGE) = NOVEC(IAGE) * NT

NT=NT+1

PRINT 934

PRINT 936

PRINT 930, (NDYLONG(J), NDXLAT(J), IAGE, J=1,NT2)

PRINT 935,NT2
               C
                                                                              00 701 J=1,NT2
                                                      100 701 J=1,NT2

ICONT IS THE PACKED HORD OF COORDINATES IN X-Y UNITS( LONG.=24 BITS, L 24 BITS, AGE=12 BITS, ALL RIGHT JUSTIFIED

100 ICONT(J) = SHIFT(NOYLONG(J) , 36).OR. SHIFT(NDXLAT(J),12).OR.1AGE R(J)=SCRI( (NDXLAT(J)-XP)**2 + (NOYLONG(J)-YP)**2 )

1F(R(J)=SCRI( (NDXLAT(J)-XP)-XP) + (R(J)-RCP48) / (R(J)-RCP48) / (R(J)-RCP50-R(J)) / (R(J)-RCP50-R(J) / (R(J)-RCP50-R(J)) / (R(J)-RCP50-R(J) / (R(J)-RCP50-R(J)) / (R(J)-RCP50-R(J)) / (R(J)-RCP50-R(J) / (R(J)-RCP50-R(J)) / (R(J)-
      C
               CC
                                                                         616,620
+A 7 )/B 7 )
+A 8 )/B 8 )
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   8)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          621,625
+A 8 1/B 8 1
+A 9 1/B 9 1
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         625,630
+A 9 1/8 9 )
+A 101/8 10)
                                                                           LONG(J) = (9.0+D1(J)/(D1(J)+D2(J)))*1000

GO TO 700

IF(SLOPE(J).GE.SLOME 10 .AND.SLOPE(J).LT.SLOME 11 )

D1(J)=ABS( (SLOME 10 *NDXLAT(J) - NDYLONG(J)

LONG(J)= [1D.0+D1(J)/(D1(J)+D2(J)))*1000

GO TO 700

IF(SLOPE(J).GE.SLOME 11 .AND.SLOPE(J).LT.SLOME 12 )

D1(J)=ABS( (SLOME 11 *NDXLAT(J) - NDYLONG(J)

LONG(J)= (11.0+D1(J)/(D1(J)+D2(J)))*1000

GO TO 700

IF(SLOPE(J).GE.SLOME 12 *NDXLAT(J) - NDYLONG(J)

LONG(J)= (11.0+D1(J)/(D1(J)+D2(J)))*1000

GO TO 700

IF(SLOPE(J).GE.SLOME 12 .AND.SLOPE(J).LT.SLOME 13 )

D1(J)=ABS( (SLOME 12 *NDXLAT(J) - NDYLONG(J)

LONG(J)= (12.0+D1(J)/(D1(J)+D2(J)))*1000

GO TO 700

IF(SLOPE(J).GE.SLOME 13 .AND.SLOPE(J).LT.SLOME 14 )

D1(J)=ABS( (SLOME 13 *NDXLAT(J) - NDYLONG(J)

LONG(J)= (13.0+D1(J)/(D1(J)+D2(J)))*1000

GO TO 700

IF(SLOPE(J).GE.SLOME 13 .AND.SLOPE(J).LT.SLOME 14 )

D1(J)=ABS( (SLOME 13 *NDXLAT(J) - NDYLONG(J)

LONG(J)= (13.0+D1(J)/(D1(J)+D2(J)))*1000

GO TO 700

IF(SLOPE(J).GE.SLOME 14 .NDXLAT(J) - NDYLONG(J)

LONG(J)= (SLOME 14 *NDXLAT(J) - NDYLONG(J)

D2(J)=ABS( (SLOME 13 *NDXLAT(J) - NDYLONG(J)

LONG(J)= (SLOME 6 *NDXLAT(J) - NDYLONG(J)

LONG(J)= (SLOME 6 *NDXLAT(J) - NDYLONG(J)

D2(J)=ABS( (SLOME 6 *NDXLAT(J) - NDYLONG(J)

D2(J)=ABS( (SLOME 7 *NDXLAT(J) - NDYLONG(J)

D2(J)=ABS( (SLOME 6 *NDXLAT(J) - NDYLONG(J)

D2(J)=ABS( (SLOME 7 *NDXLAT(J) - NDYLONG(J)

D2(J)=ABS( (SLOME 6 *NDXLAT(J) - NDYLONG(J)

D2(J)=ABS( (SLOME 7 *NDXLAT(J) - NDYLONG(J)

D2(J)=ABS( (SLOME 7 *NDXLAT(J) - NDYLONG(J)

D2(J)=ABS( (SLOME 7 *NDXLAT(J) - NDYLONG(J)

D2(J)=ABS( (SLOME 6 *NDXLAT(J) - NDYLONG(J)

D2(J)=ABS( (SLOME 7 *NDXLAT(J) - NDYLONG(J)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            631,635
+A 10)/B 10)
+A 11)/B 11)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         636,640
+A 11)/B 11)
+A 12)/B 12)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         641,645
+A 12)/B 12)
+A 13)/B 13)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            646,650
+A 13)/B 13)
+A 14)/B 14)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          +A 13)/B 13)
+A 14)/B 14)
                    655
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          +A 6 1/B 6 1
+A 7 1/B 7 1
                                       LONG(J) = ( 6.0-01(J)/(02(J)-01(J)))*1000

69 TO 700

693 PRINT 994
```

```
APPROXIMATION FOR LONG(J) WHOSE SLOPE IS UNDETERMINED LONG(J)=LONG(J-1)
700
701
                           NGEO(J)=SHIFT(LONG(J),36).OR.SHIFT(LAT(J),12).OR.IAGE CONTINUE
 CCC
                           PRINT 950, (R (J), SLOPE(J), D1(J), D2(J), J=1, NT2)
    PRINT 950, (R (3), SLOPE(3), D1(3), D2(3), J=1,NT2)

PRINT 94

PRINT 951, (LONG(J), LAT(J), J=1,NT2)

WRITE(8, 2237) IF EATNO, LONG(1), LAT(1), IAGE, NT2

NXX(1) = IF EATNO$N XX(2) = LONG(1) $N XX(3) = LAT(1) $N XX (4) = IAGE $N XX (5) = NT2

BUFFEROUT(2, 1) (NXX(1), NXX(5)) $IF (UNIT(2)) 1791, 1791

1791 BUFFEROUT(2, 1) (NGEO(1), NGEO(NT2)) $IF (UNIT(2)) 1792, 1792, 1792

1792 CONTINUE
  č
                           IF(IRECHO.LT.NUMREC)70,1000
CONTINUE
                           PRINT 938, (I, NOVEC(I), I=1, 148)
   PRINT 938, (I, NO VEC (I), I=1,148)
END
SUBROUTINE INGGC 6 (IEOF, NOWORD)
THIS VERSION OF INGGC IS FOR THE 6 DEGREE TAPE
COMMON / INPUT / IRECNO, NUMVEC, IXST, IYST, IVEC (6000), IRECTYP, IFEATNO
COMMON IBLKNO, ISTVEC, IAGE, INOLD (1080), IRECRES, L, NOF TREC
COMMON XP, YP, RCP (50), SLOMER(20), A(10), 8(10), AA(10), BB(10), CC(10),

Z DD(10), D485 0, D5052, D5254
DIMENSION JGGC (69), LX (20), LY (20), DL (19), DC P50 (5), PHI (15)
TYPE REAL LX, LY
5 FORMAT (4(2X, P1E16.8))
8 FORMAT (4(2X, P1E16.8))
8 FORMAT (4(2X, P1E16.8))
9 FORMAT (4(2X, P1E16.8))
143 FORMAT (4(2X, P1E10.4))
144 FORMAT (5(2X, I2, 2(2X, F7.1)))
145 FORMAT (5(2X, I2, 2(2X, F7.1)))
146 FORMAT (5(2X, I2, 2X, P1E18.10))
200 FORMAT (5(2X, I2, 2X, P1E18.10))
200 FORMAT (2X, *XP=*P1E14.7, 2X, *YP=*P1E14.7)
436 FORMAT (* FILE SUMMARY RECORD *)
496 FORMAT (* ENO OF FILE*)
1000 FORMAT (* INVALID AECORD TYPE*)
1000 FORMAT (* INVALID AECORD TYPE*)
1500 FORMAT (* INVALID AECORD TYPE*)
1500 FORMAT (* INVALID AECORD TYPE*)
 CC
                        READ NEW RECORD
BUFFER IN (1,1) (JGGC(1), JGGC(69))
TEST IF E OF OR PARITY ERROR WAS ENCOUNTERED ON TAPE
IF (UNIT(1)) 120,495,110
PRINT 1500
IEOF=0
      100
 C
          105
         00 140 1=1,19

J=8*I +253

LX(1)=INOLD(J)*4096+INOLD(J+1)*256+INOLD(J+2)*16+INOLD(J+3)

LY(1)=INOLD(J+4)*4096 +INOLD(J+5)*256 +INOLD(J+6)*16 +INOLD(J+7)
   140 LY(1)=INOLO(J+4)*4096 *INOLO(J+5)*256 *INOLO(J+6)*16 *INOLO(J+7)
PRINT 143
PRINT 144, (I, LX(I), LY(I), I=1,19)
XPN=(LX(5)*LX(19))*(LY(5)-LY(19))+(LX(5)*LX(19))*(LY(19)-LY(15))+
A (LX(9)*LX(15))*(LY(5)-LY(19))+(LX(15)*LX(19))*(LY(19)-LY(5))
XPD=(LY(15)-LY(5))*(LX(19)-LX(9))-(LX(15)-LX(5))*(LY(19)-LY(9))
XP=XPN/XPD
YP = LY(5)+(XF - LX(5))*(LY(15)-LY(5))/(LX(15)-LX(5))
D1 1441 M=5,14
D1 1441 M=5,14
D1 M)=SQRT((LX(M+5)-LX(M))**2 + (LY(M+5)-LY(M))**2)
D1 2554=(DL(10)+DL(11)+DL(13)+DL(14))/5.
PRINT 8,(DL(M), M=5,14)
PRINT 8,(DL(M), M=5,14)
PRINT 146,(I,RCF(I),I=1,19)
145 RCP(I)=SQRT((LX(M+5)-LX(M+4))**2 + (LY(M+5)-LY(M+4))**2)
DCP50 (M)=SQRT((LX(M+5)-LX(M+4))**2 + (LY(M+5)-LY(M+4))**2)
```

```
1443 PHI(M) = ( ASIN(DCP50(M)/RCP(M+4)))*(180./3.14159)
PRINT9,(PHI(M), M=1,4)
 IF(IAGE+GT.0.AND+IAGE+LT.10.)500,188
IAGE=0
PRINT 1000
G0 T0 500
IF(IRECTYP+EG.31) 190,430
STARTING VECTOR POSITION NUMBER USUALLY "28"
ISTVEC=(INOLD(14)-AND.07B)*(2**8) + INOLD(15)*(2**4) + INOLD(16)
NUMVEC=(INOLD(18).AND.07B)*(2**8) + INOLD(19)*(2**4) + INOLD(20)
IXST = (INOLD(21)*(2**12) + INOLD(22)*(2**8) + INOLD(23)*(2**4)
1 + INOLD (24)
IYST = (INOLD(25)*(2**12) + INOLD(26)*(2**8) + INOLD(27)*(2**4)
1 + TNOLD(28);
       189
C 190
                                       + INOLD(28);
L=NOFTREC-IBLKNO
GO TO 500
IF(IRECTYP-EQ.90)435,450
         430
                                     PRINT 436
NUMFEAT=INOLD(21)*(2**12)+INOLD(22)*(2**8)+INOLD(23)*(2**4)+INOLD(
                                 $24)
NUMBLK S=INOL D(25) *(2**12) + INOL D(26) *(2**8) + INOL D(27) *(2**4) + INOL D(
         NUMBLKS=INOLD(25)*(2**12)*INOLD(26)*(2**6)*TINOLD(26)*(2**6)*TINOLD(26)*(2**6)*TINOLD(26)*(2**6)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TINOLD(26)*TI
END

6999

MC6GS,T160,CM145000,TP2.

FTN,SL,A,P,BL,R=3,PL=49999,T.

MAP(ON)

VSN,TAPE1=0S0139.

RE OUEST,TAPE1,HY,L.

VSN,TAPE4=050172.
                                                                                                                                                                                                                                                                                                                     2096
                                                                                                                                                                                                                                                                                                                                                                        MCCOMISH
```

6. DESCRIPTION OF PART IV

6.1 Overview

The purpose of PART IV of the LORAN Grid Prediction Program is to update the input data base to PART II. By comparing the time differences at measured and calculated fixed points in the service area, corrections are applied to the postulated top soil conductivity values to zero out the difference between the former. A technique described by Elkins ²² has been utilized which employs a continuous Kalman filter with updating of references state vector. The details of this program are described in Program ESTIMAE. ²³ It is pointed out that of the nine parameters required to calculate the surface impedance, only the two predominant top soil conductivities are altered.

The approach taken for system tuning or data base updating is as follows:

- (1) Compute time difference in PART III of Program for locations for which measured data is available.
- (2) Identify two values for top soil conductivity that occur most frequently in the geographical area of interest.
- (3) The variation in the LORAN time difference due to a variation in topsoil conductivity is computed by changing in turn, each of the two conductivity values where they occur in the geographical area of interest and proceeding with the step outlined in "1" above.
- (4) The difference between the observed and calculated data, the rates of change in time difference due to changes in each conductivity value, estimate of the error in the initially chosen values of conductivity, and estimates of the error in the observations are input to a Kalman filter program to produce an improved estimate of the value of conductivity.
 - (5) The improved values of conductivity are written into the data base.

For the test program, the conductivity was changed by 10 percent to form the required partial derivatives; absolute conductivity was estimated within a factor of two, and the standard deviation of the time difference measurement was assumed to be 100 μ sec. Utilizing forty test points, this technique reduced the prediction errors by 33 percent.

A listing of the program is presented below.

^{22.} Elkins, T.E. (1976) Empirical Correction of Soil Conductivity Model, RADC/ET Private Communication.

^{23.} Program ESTIMAE - Problem No. 4723 (1975) Analyses and Simulation Branch, AFCRL dated 1 November 1975.

```
I ESTMATE
             74/74
                     OPT=1
                                                         FTN 4.5+414 06/20/77
       PROGRAF ESTMATE(INPUT=4018, OUTPUT=4018, TAPE1=4018, TAPE2=4018,
     1 TAPE3=4018, TAPE4=+018, TAPE10, TAPE11, TAPE20=11018)
C.... GIVEN (1) A SET OF DIFFERENTIAL EQUATIONS DESCRIBING A DYNAMICAL
  SYSTEM, (2) AN ESTIMATE OF THE STATE OF THE SYSTEM AT SOME INITIAL
   TIME ALONG WITH STATISTICS PROVIDING A MEASURE OF THIS ESTIMATE.
   AND (3) A DATA FILE CONTAINING OBSERVATIONS BEARING ON THE STATE OF
   THE SYSTEM AT SPECIFIED POINTS OF TIME. COMPUTE THE BEST ESTIMATE OF
   THE STATE OF THE SYSTEM ALONG WITH SOME STATISTICS GIVING A MEASURE OF THE ESTIMATE AT EACH OF THE SPECIFIED POINTS OF TIME. THE BEST
   ESTIMATE IS BASED ON ALL OBSERVATIONS PROCESSED UP TO THE CURRENT
   TIME. A BACKWARD SMOOTHING FEATURE IS PROVIDED AS AN OPTION SO THAT
   THE ESTIMATES AT THE FIRST ( POINTS OF TIME WILL REFLECT THE
   INCLUSION OF ALL OBSERVATIONS UP TO THE K IH POINT OF TIME.
       COMMON/CASE/CASE
       COMMON/RK/TI, TF, NRC4578, SDT, DT, TOL, SP, NERR1, NERR2, ORD,
      1 NSTEP, NKEJ, IST 21
       COMMON/STREF/IXR,XR(1)
       COMMON/STESTM/IXE, (E(1)
       COMMON/STRSDL/IX,X(1)
       COMMON/STCOV/IP, JP, P(1)
       COMMON/STNCOV/ IQ, QCOV
       COMMON/OBSH/IH, JH, H(1)
       COMMON/OBSY/IY, Y(1)
       COMMON/OBSCOV/IR,R(1)
       COMMON/MEASCOV/RCOV(6)
       COMMON/PARAMS/KSTRSDL, HSTEP, TIMETOL, KOUNCH, KREW IND, TOLRNCE, IDER,
      1 KPLOT, KEND, KONE, KS, KSMOUTH, MAXS, MAXKZ, MPTY, NGPS, NLRSR, NLRSW,
      2 NFILF, NFILB, NSAT, NNSAT, NGPS1, NGPS2, NRSEQ, NRRAN, NWSEQ, NWRAN, NPRAN,
      3 IOB, JZH, IST, IS1, IS2, KORIT, KC BEGIN, KPRINT, KWRIFE, KO ATA, KTYPES,
      4 MAXDATA,IA,JA,KA,IM,JM,KM,MD,KPLWD,IFYPES(2),PRINMOM(3),KQKLOCK,
     5 IDERSET
C.... THE FOLLOWING COMMUN AND EQUIVALENCE STATEMENTS ARE DEPENDENT ON
  THE DATA FILE USED.
       COMMON/BUFF/LBUFF(+),TIME
       DIMENSION ID(1) $ EQUIVALENCE (D, ID)
       COMMON D(36), XRU(12), S(144)
       DIMENSION XO(12) ,DIAGJ (12)
       EXTERNAL DER
       NA MEL IST/VALUES/CASE, TSTART, TSTOP, Xu, JIAGO, KPLOT, KPRINT,
      1 KWRITE, KRE WIND, KS 400TH, MAXS, KCRIT, MAXKS, KCBEGIN, KTYPES, MAXDATA,
      2 IA, JA, KA, IM, JM, KM, NRK4578, STEP, TOL RNCE, SP, NERR1, NERR2, ORD, IST,
      3 IS1, IS2, JZH, KSTRS)L, QCOV, RCOV, TIMETO_, KPARTS, KPL WD, MD, RUNMAX,
      + KQKLOOK
C.... KEAD IN INITIAL PARAMETERS.
                                      CALL SUBROUTINES TO SET INITIAL
   PARAMETERS AND TO SELECT OPITONS.
     1 CASE=CASE+1. $ READ VALUES
       IF (CASE.LT. L.) 46,2
     2 CALL FILEIO(1)
       CALL OBSERVE
       CALL STATS
       CALL PACK (KPL HD, I, I)
       SUT=STEP
                 $ TOL = TO_RNCE
       IDER=0
C.... SET REFERENCE STATE VECTOR AND DIAGONAL STATE COVARIANCE MATRIX TO
C INITIAL CONDITIONS.
       CALL DIAGNAL(IST, X), XR, DIAGO, IP, P)
```

C.... SET MAXIMUM RUN-TIME LIMIT.

```
CLOCKO=SECOND(T)
C.... PRINT INITIAL PARAMETERS.
PRINT VALUES
C.... SET START AND STUP TIMES.
      TI=TSTART
      IST1=IST+1 $ IST21=IST*IST1
C .... READ IN THE NEXT DATA RECORD.
    3 CALL FILEIO1(TI), RETURNS (4,42)
    4 IF (TIME.GT. TSTOP)5,8
    5 KEND=1 $ GO TO +2
C.... TIME OF DATA RECORD LIES WITHIN REQUESTED INTERVAL.
    8 I=IIME $ KOP=0
   11 TF=T
     HSTEP = ABS (TF-TI)
C.... TEST WHETHER OR NOT TI AND TE ARE APPROXIMATELY EQUAL.
  14 IF (HSTEP.LE.FIMETO_) 21,15
C.... INTEGRATE FORWARD TO TF.
  15 IF (KOP) 19,16
C.... NAP THE STATE COVARIANCE MATRIX FORWARD.
   16 CALL MATRIX (0, 1ST, 1ST, 0, 2, 1P, XR(1ST1), 1ST, 0,0)
      IDERSET=2 $ CALL RK4578(XR, DER)
      CALL MATRIX (0, IST, [ST, 0, XR (IST1), IST, 2, IP, 0,0)
      GO TO 21
   19 IF (KRESET. EQ. 1) GO TO 20 $ KRESET = 1
      CALL MOVLEV(XR, XRJ, IST)
   20 CALL RK4578 (XR, DER)
   21 TI=TF
C.... SELECT THE DATA FROM THE RECORD.
      IF (KOP. LQ. u)22,25
   22 CALL OBSERV1 $ IDB=0 $ ITYPES(1)=ITYPES(2)=1H
23 KOP= KOP+1 $ IF(K)P.GT. (DATA) 36,24
   24 N=MD+(KOP-1)+1 5 T=D(N) $ I=ID(N+2)
      IF (KOP. EQ. 1)80.11
C.... INITIALIZE STATE FRANSITION MATRIX.
   80 00 10 M=1, IST $ L=IST*4 $ DO 9 K=1, IST $ J=K+L
    9 XR(J)=0. $ J=M+_
   16 XR(J)=1.
      KRESET = 0
      1DERSET=1 $ GO TO 11
C.... ENTER APPROPRIATE SUBROUTINE TO FIND THE COMPUTED OBSERVATION. THE
 DIFFERENCE BETWEEN THE GIVEN OBSERVATION AND THE COMPUTED
C OBSERVATION, AND THE PARTIALS OF THE COMPUTED OBSERVATIONS.
   25 IF (I.EQ.1) 26,27
   26 CALL SSENSOK(KPARTS, D(N), S) $ GO TO 35
   27 1F (I.EQ. 2) 28,29
   28 CALL ESENSOR(KPARTS, D(N), S) $ GO TO 35
   29 1F (4. LE. I. AND. I. LE. 6) 3u, 31
   30 CALL MAGDATA(KPARTS, D(N), S) $ GO TO 35
   31 1F (I. EQ. 16) 34, 36
   34 CALL ACCEL (KPARTS, ) (N), S)
C.... SAVE DESERVATION TYPES FOR PRINTOUT.
   35 IF (KPRINT. AND. >12) 530,23
  530 J=3*KOP-1 $ ENCODE (16, 31, S) J
  531 FORMAT (10H(T1, 2A13, T, 12, +H, 12))
      ENCODE (20, S, ITYPES) ITYPES, I
      GO TO 23
   36 11=11ME $ IF(108)37,41
```

37 IF (KRESET. EQ. 1) CALL MOVLEV (XRE, XR, IST) C.... ENTER THE FILTER. IF (KONE) 38, 39, 39 38 NFIL8=NFIL8+1 \$ 30 TO +0 39 NFILF=NFILF+1 40 CALL FILTER, RETURNS (44) C.... COMPUTE THE BEST ESTIMATE. GALL MATRIX(21, ISI, 1, 3, XR, IXR, X, IX, XE, IXE) C.... DETERMINE PRINCIPAL VALUES OF ANGLES. 4000 UO 400 I=1,3 400 X= (I) = PRINVA_ (XE (I)) C.... REINITIALIZE STATE REFERENCE VECTOR. CALL NOVLEV (XE, XR, [ST) C.... CHECK FOR MAXIMUM RUN TIME.

CLOCK=SECOND(T)-CLOCKU & IF(CLOCK.GF.RUNMAX) KEND=1 C.... GATHER APPROPRIATE STATISTICS ON THE ESTIMATION. CALL STATS1 IF (KEND. EQ. 6) CALL FILEID2 (TI), RETURNS (4,42) C.... INITIATE END PROCESSING. 42 CALL FILEIO3(T) 43 GO TO 1 44 PRINT 45 , NGPS , KONE 45 FORMAT (*OSINGULAR MATRIX ENCOUNTERED. 5 X FGROUP= #14, 5X FKONE= #12) C.... SIMPLY EQUATE BEST ESTIMATE VECTOR AND STATE REFERENCE VECTOR. 41 CALL MOVLEV (X2, XE, [ST) 5 DO 450 K=1, IST 450 X(K)=0. \$ 30 TO +000 46 CONTINUE \$ END

N PRINVAL 74/74 UPT=1

FTN 4.5+414

FUNCTION PRINVAL (ANGLE)

C.... PRINVAL RETURNS THE PRINCIPAL VALUE OF THE GIVEN ANGLE.

C (- PI .LT. PRINVAL PI)

DATA PI/3.141592693589793/
A=ANGLE

1 AA=ABS(A) \$ 1F(A4.LE.PL) GO TO 2
A=A-SIGN(2.*PI,A) \$ GO TO 1
2 PRINVAL=A \$ KETURN \$ END

```
SUBROUTINE STATS
C.... RECORDS STATISTICS IN ORDER TO EVALUATE THE PERFORMANCE OF THE C ESTIMATION PROCESS. CONTROLS THE INITIATION OF THE BACKWARD
 SMOOTHING PROCESS AND THE ASSOCIATED RANDOM FILE WRITING. CONTROLS
  ALL PRINTED OUTPUT ON FILES 1,2,3, AND 4.
      COMMON/STREF/IXR,XR(1)
      COMMON/STESTM/IXE, XE(1)
      COMMON/STRSDL/IX,X(1)
      COMMON/STCOV/IP, JP, P(1)
      COMMON/SICOVD/IPD, )(1)
      COMMON/OBSY/IY, Y(1)
      COMMON/PARAMS/1Q(7), KPLOT, KEND, KONE, KS, KSMOOTH, MAXS, MAXKC, MPTY,
     1 NGPS, NLKSR, NLRSW, NFILF, NFILB, NSAT, NNSAT, NGPS1, NGPS2, NRSEQ, NRRAN,
     2 NWSEQ, NWRAN, NPRAN, IOB, JZH, IST, IS1, IS2, KCRIT, KCBEGIN, KPRINT, KWRITE
     3 , JQ(11) , OBTYPES (2)
      COMMON/CRIT/CRIT(1)
      THE FOLLOWING COMMON AND EQUIVALENCE STATEMENTS ARE DEPENDENT ON
C THE DATA FILE USED.
      COMMON/BUFF/LBUFF(+), W(127)
       DIMENSION XT(1) $ EQUIVALENCE (W, TIME), (W(10), XT)
      COMMON DX(12), XD(12), IS(24),0(50)
       DIMENSION S(1) $ EQUIVALENCE (IS, S)
      LOGICAL NRSER, NRRAY, NWSER, NWRAN, NPRAN
      DATA MAXK/5/, MORE/5H MORE/
C.... SET INITIAL CONSTANTS.
      NLRSR=NLRSW=NGPS=NFILF=NFILB=NSAT=NNSAT=KST=KEND=C
      NRSEQ = . T. S NRRAN = NWSEQ = NWRAN = NPRAN = . F.
      KS=KSMOOTH
                   3
                      KONE = 1
      SET PRINT OPTIONS.
                            AT MUST 1 OPTION PER FILE IS ALLOWED.
C KPRINT BIT U.
                   PRINT TIME, STATE VECTOR ON FILE 1.
                   PRINT (IME, STATE RESIDUALS VECTOR ON FILE 2. PRINT (IME, STATE DEVIATIONS VECTOR ON FILE 2.
   KPRINT BIT 1.
   KPRINT BIT 2.
   KPRINT BIT 3.
                   PRINT FIME, STATE DERIVATIVES VECTOR ON FILE 2.
   KPRINT BIT 4.
                   PRINT TIME, DIAGONALS OF STATE COVARIANCE MATRIX ON
   FILE 3.
   KPRINT BIT 5.
                   PRINT FIME, STATE COVARIANCE MATRIX ON FILE 3.
                   PRINT (IME, TORQUES ON FILE 3. PRINT COMPLETE STATISTICS ON FILE 4.
   KPRINT BIT 6.
   KPRINT BIT 7.
                   PRINT PARTIAL STATISTICS ON FILE 4. (KCRIT. NE. L)
   KPRINT BIT 8.
   KPRINT BIT 9.
                   PRINT TIME, SOME STATISTICS, AND OBSERVATION RESIDUALS
   VECTOR ON FILE 4.
      IF (KPRINT) 2,1
    1 ASSIGN 55 TO M1 $ GO TO 17
    2 CALL WRITERO(4,0,0)
      ASSIGN 41 TO M1 $ ASSIGN 46 TO M2
ASSIGN 52 TO M3 $ ASSIGN 55 TO M4
      ASSIGN 541 TO M41
C.... SET PRINT LIMITS ON STATE VECTOR ELEMENTS.
       IS2=MINU(12,IS2,ISF, (IX-IS1+1)) $ IS4=IS1+IS2-1 $ IS3=IS2+1
      PRINT 16, (I, I= IS1, IS4)
       PRINT 160 $ PRINT 161
       I = J= 1
    3 K=KPRINT.AND.J $ IF(KcNE.0) GO TO (5,5,7,9,10,11,13,14,14,15),I
    4 J=2*J $ I=I+1 $ IF(I.GT.16)17,3
    5 ASSIGN 40 TO MI
                         8
                             GO TO 4
    6 ASSIGN 42 TO M2 3
                            GO TO 4
    7 ASSIGN 43 TO M2 $ GO TO 4
```

```
9 ASSIGN 44 TO M2 & GO TO 4
   10 ASSIGN 47 TO M3 $ GO TO 4
   11 ASSIGN 48 TO M3
                            GO TO 4
   13 ASSIGN 51 TO M3 8 GO TO 4
   14 KSi=1
  140 ASSIGN 54 TO M4
      1F(I. LQ. 9) ASSIGN 53 TO M4 $ GO TO +
   15 ASSIGN 540 TO M41 $ GO TO 140
   16 FORMAT (*1DESCRIPTION OF PRINTOUTS ON FILES 1, 2, OR 3*/5X*ONLY THE
     1 FOLLOWING COMPONENTS OF THE STATE VECTOR, STATE RESIDUALS VECTOR,
     2 STATE DEVIATIONS VECTOR, STATE DERIVATIVES VECTOR OR THE*/* FOLLO BHING COLUMNS OF THE STATE COVARIANCE MATRIX OR THE FOLLOWING DIAGO ANAL ELEMENTS OF THE STATE COVARIANCE MATRIX ARE PRINTED OUT.*/1X,
     512 [5]
  160 FORMAT(* FOR THE UBSERVATION RESIDUALS VECTOR, ALL COMPONENTS, AS
     INELL AS THE OBSERVATION TYPES, ARE PRINTED OUT. +)
  161 FULMATI
     5*-DESCRIPTION OF STATISTICS PRINTOUT ON FILE 4*/5x*GP....POSITION
     70F DATA GROUP WRT FIRST DATA GROUP PROCESSED*/5X*LR R....LUCATION
     BOF LOGICAL RECORD OF DATA WAT FIRST LOGICAL RECORD READ*/5X
     9*LK W....CUMULATIVE NUMBER OF LOGICAL RECORDS WRITTEN TO OUTPUT DA
     ATA FILE
                        */5x*F F....CUMULATIVE NUMBER OF TIMES ENTERED FIL
     BTER FOR FORMARD FILTERING*/5X*F B....CUMULATIVE NUMBER OF TIMES EN
     CTERED FILTER FOR BACKWARD SMOOTHING */5 X*SAT .... CUMULATIVE NUMBER O
     DE TIMES PERFORMANCE CRITERIA SATISFIED*/5X*NSAT....CUMULATIVE NUMB
     EER OF TIMES PERFORMANCE GRITERIA NOT SATISFIED*/5X*ELEMENT....RELA
     FTIVE ECCATION WITHEN STATE OR STATE RESIDUAL VECTOR*/5X*VALUE....T
     GEST VALUE WHICH EXCEEDED SPECIFIED CRITERIA*/5X*MORE....FLAG IMPLY
     HING THAT MORE ELEMENTS FAILED TEST*/5X*FIME....TIME OF DATA GROUP*
     I)
   17 ASSIGN 18 TO M6
C.... SET CRITERIA OPTIONS.
C KCKIT BIT G. COVARIANCE LIMIT CRITERIA.
C KCRIT BIT 1. COMPARISON WITH EXISTING STATE CRITERIA.
      ASSIGN 37 TO M5
      IF (KCRIT.LQ.1) ASSIGN 21 TO M5
      IF (KCRIT. EQ. 2) ASSIGN 22 TO M5
C.... SET SEQUENTIAL WRITE OPTION.
      IF (KWRITE. EQ. 1) NWSEQ = . NOT . NWSEQ
      KETURN
      ENTRY STATS1
C.... USUAL ENTRY POINT INTO STATS.
      GO TO M6, (18, 20)
C.... WHEN PROCESSING FIRST DAIA GROUP, SPECIFY NECESSARY OPTIONS.
   18 ASSIGN 26 TO Mo
      IF (KPLOT. EQ. 1) NPRAN = . NOT. NPRAN
      IF (KSMOOTH) 19, 20
   19 NWKAN=.NOT.NWRAN $ NWSEQ=.NOT.NWSEQ $ NPRAN=.NOT.NPRAN
      LGPNS=G
C.... CHECK WHETHER OR NOT CRITERIA ARE SATISFIED.
   20 K= 6 $ 00 26 I=1, IST $ GO TO M5, (21, 22, 37)
   21 J=1+IP*(I-1)
                     *
                        VAL=P(J) $ GO TO 220
   22 JAL=XE(I)-XT(I)
  220 IF (ABS (VAL) .LE. CRIF (I))25,23
23 K=K+1 $ IF(KST)2+,36
C... SAJE DATA ON ELEMENTS NOT SATISFYING CRITERIA.
   24 IS(K)=I $ K=K+1 $ S(()=VAL $ IF(K.GT.2*MAXK)25,26
```

```
25 K=K-1 $ IS(K)=MORE $ GO TO 36
26 CONTINUE $ IF(K)36,27
27 NSAT=NSAT+1 $ IF(KS.EQ.1)28,39
   28 IF ((NGPS-LGPNS) . GE, MAXKC) 29, 31
C.... MAXKC CONSECUTIVE SATISFACTORY ESTIMATES.
   29 IF (LGPNS) 34,35
C.... BACKWARD SMOOTHING NECESSARY.
   30 NGPS1=NGPS-KOBEGIN $ N_RSR=NLRSR-KC3EGIN $ GO TO 33
   31 IF (NGPS.GE. MAXS) 32,39
   32 N3P51=NGPS
   33 KONE = -1
   34 NGPS2=NGPS $ KS=-1
      NRSEQ=.NOT.NRSEQ & NRRAN=.NOT.NRRAN & GO TO 39
C .... BACKWARD SMOOTHING NOT NECESSARY.
   35 NGPS1=1 $ NLRSR=VLRSR-VGPS+1 $ GO TO 34
C .... AN UNSATISFACTURY ESTIMATE.
   36 NNSAT=NNSAT+1 $ _GPNS=NGPS
   37 IF (KS.EQ.1) 31,39
C.... EXTRACT DIAGONAL PORTION OF COVARIANCE MATRIX.
  39 DO 390 I=1, IST
  390 D(I)=P(I+IP*(I-1))
      CALL MATKIX (22, IST, 1, 0, XE, IST, XT, IST, KD, IST)
C.... PRINT SELECTED INFORMATION ON OUTPUT FILES.
      0(1)=TIME $ GO () M1,(+0,41,55)
   46 CALL MOVLEV (XE(IS1), 0(2), IS2) $ CAL. HRITER (1, 2, IS3)
   41 GO TO M2, (42, 43, 44, 46)
   42 GALL MCVLEV (X(IS1), 0(2), IS2) $ GO TO 45
43 GALL MCVLEV (XD(IS1), 0(2), IS2) $ GO TO 4
                                          $ 50 10 45
   44 CALL MOVLEY (DX (IS1), 0(2), IS2)
   45 CALL WRITER (2, 0, 153)
   40 GO TO M3, (47, 40, 51, 52)
   47 CALL MCVLEV (U(151), 0(2), 152) $ L=IS3 $ GO TO 50 48 L=1 $ UO 49 I=IS1, IS4 $ DO 49 J=IS1, IS4 $ L=L+1
   49 O(L)=P(1+IP*(J-1)) $ G) TO 50
   50 CALL WRITER (3, U, L)
   51 CONTINUE
   52 GO TO M4, (53, 54, 55)
   53 1F (K) 54,55
   54 CALL MCVLEV (NGPS, 0(2),7) $ GO TO M41, (540,541)
  546 K=6 $ IF(108.EQ. )) GO 10 542
       CALL MCVLEV(OBTYPES, O(9), 2) $ CALL 40VLEV(Y, O(11), IOB)
       K=2+108 $ GO TO 542
  541 CALL MOVLEV(IS, 0(9), K)
  542 CALL WRITER (+, 0, 8+ ()
   55 IF (NPRAN. AND. . NOT. NWRAN) 56,57
C.... SAVE DATA FOR EVENTUAL P.OTTED OUTPUT.
   56 CALL MOVLEV (XE,O(2),IST) $ I=2+IST CALL MCVLEV (X,O(I),IST) $ I=I+IST CALL MCVLEV (XO,O(I),IST) $ I=I+IST
       CALL MOVLEV (D, ) (I), IST) $ I=I+ISI-1
       CALL PACK1(I,0,MPT/)
   57 RETURN $ END
```

```
SUBROUTINE FILEIO(1), RETURNS (NR1, NR2)
      THIS ROUTINE IS THE CONTROLLING ROUTINE FOR ALL FILE INPUT AND
 OUTPUT IN THE PROGRAM.
      COMMON/STREF/IXR, XR(1)
      COMMON/STESTM/IXE, (E(1)
      COMMON/STCOV/IP, JP, P(1)
      COMMON/STCOVD/IPD, D(1)
      COMMON/RANFILE/MAXMS, MS(1)
      COMMON/PACKED/NLRS, NHORDS, NH (512)
      EQUIVALENCE (WH, IW41), (WH(2), IWW2)
      COMMON/PARAMS/KSTREDL, HSTEP, TIMETOL, KOUNCH, KREWIND, LRWOCHT(2),
     1 KPLOT, KEND, KONE, KS, KSMO)TH, MAXS, MAXKC, MPTY, NGPS, NLRSR, NLRSH,
     2 NFILE, NFILB, NSAT, NNSAT, NGPS1, NGPS2, NR SEQ, NRRAN, NWSEQ, NWRAN, NPRAN,
     3 IOB, JZH, IST, Z1(22), KQKL) OK
C.... THE FOLLOWING COMMON AND EQUIVALENCE STATEMENTS ARE DEPENDENT ON
C THE DATA FILE USED.
      COMMON /BUFF/LENGTHR, LENGIHW, MAXLRW, LRW, W (127)
      EQUIVALENCE (W, TIME)
      COMMON RECORD(14)
      LOGICAL NRSEQ, NRRAN, NWSER, NWRAN, NPRAN
      DATA KOPEN/-1/
C.... SET FILE INPUT/OUTPUT OPTIONS.
      IF (KSMOOTH.NE. O. OR, KPLOT. NE. O) KOPEN=COPEN+1
      IF (KOPEN) 101, 102, 1)1
  102 CALL OPENMS (20, MS, 4AXMS+1,0) $ KDPEN=KOPEN+1
  101 MAXS=MIND(MAXS, MAX4S) $ MAXKC=MIND(MAXKC, MAXS)
      IF (KREWIND.NE. 0) REWIND 10
      ASSIGN 36 TO M1
      KREWRIT=0
      RETURN
      ENTRY FILEIOL
C .... RANDOM FILE READ.
  100 IF (NRRAN) 1, 15
    1 IF (KS) 2,8,15
    2 IF (NGPS1.EQ.1) 3,6
C.... BACKWARD SMOOTHING EITHER NOT NECESSARY OR NOW COMPLETE.

3 KONE=1 $ KS=u $ ASSIGN 37 TO M1

NWSEQ=.NOT.NWSEQ $ NWR4N=.NOT.NWRAN $ NPRAN=.NOT.NPRAN
      IF (NGPS1.EQ.NGPS) 37,10
C.... CONTINUE WITH BACKAARD SMOOTHING.
    6 IF (NGPS. EQ. NGPS1) 3,7
    7 ASSIGN 11 TO M1 $
                            GO TO 10
    8 IF (NGPS.NE.NGPS2) 30 TO 9
C.... RESUME SEQUENTIAL FILE READ.
      NRRAN=.NOT.NRRAN $ NRSEQ=.NOT.NRSEQ
      KREWRIT =- 1 $ GO TO 11
C.... READ IN A LOGICAL RECORD.
    9 NGPS1=NGPS1+KONE & NLRSR=NLRSR+KONE
   10 CALL READMS (20, LRH, MAXLRH, NGPS1)
      LRW=LRW-2*ISI
      NGPS=NGPS1 $ GO TO M1,(11,36,37)
C.... MOVE APPROPRIATE VALUES FROM W ARRAY TO STATE AND COVARIANCE
  ARRAYS
   11 I=LRW+1 $ CALL MOVLEV(A(I), XE, IST)
I=I+IST $ CALL MOVLEV(A(I), D, IST)
      CALL DIAGNAL(IST, XE, XR, D, IP, P) $ T=FIME
      ASSIGN 36 TO M1 $ GO TO 100
```

```
C.... SEQUENTIAL FILE READ.
   15 IF (NRSEQ) 16,22
C.... KEAD IN A LOGICAL RECORD.
  16 KEAD(10) LRW, (W(I), I=1, LRW) $ NLRSR= N_RSR+1
C.... CHECK LAST BINARY READ.
      IF(IO EOF PE(18))24,17,15
   17 NLRSR=NLRSR-1
   22 KEND=1 $ RETURN VR2
C.... DATA LOGICAL RECORD.
  24 IF (TIME.LT.T-TIMET)L)49,35
C.... ACCEPTABLE DATA RECORD.
   35 NGPS=NGPS+1
   36 RETURN NR1
      ENTRY FILEIO2
C.... RANDOM FILE WRITE.
   37 IF (NWRAN) 40,41
   40 I=LRW+1 $ CALL MOVLEV(XE,W(I),IST)
I=1+IST $ CALL MOVLEV(),W(I),IST)
      LRW=LRW+2*IST
      CALL WRITMS (20, LRW, LRW+1, NGPS, KREWRIT) $ GO TO 49
C.... SEQUENTIAL FILE WRITE.
   41 IF (NWSEQ) 42,45
   42 I=LENGTHR+1 $ CALL MOV.EV(XE,W(I),IST)
I=I+LENGTHW $ CALL MOV.EV(D,W(I),IST)
      LRW=LENGTHR+2*LENGTHW
      WRITE(11) LRW, (W(I), I=1, LRW) $ NLRSH=NLRSW+1
C.... OUTPUT DATA FOR EVENTUAL PLOTTING, COMPARISON, ETC.
   45 IF (NPRAN) 46,49
   46 IF (MPTY.EQ. 1) 48,49
   48 M=NLRS+1
      CALL WRITHS (20, WH, WHORDS, M, KREWRIT) $ NWORDS=0
      IF (M. EQ. MAXMS) NPRAN= . NOT . NPRAN
   49 IF (KEND. EQ. 1) 22, 13)
      ENTRY FILEIOS
C .... PERFORM END PROCESSING.
   50 FORMAT(*-MINIMUM AVD MAXEMUM VALUES FOR DATA ON PLOT FILE.*T70*HOR
     1US PER GROUP* 14, T1) 0 * TOTAL LOGICAL RESORDS* 14/)
   51 FORMAT (14,2X,1P2E2).12)
   53 IF (KPL CT) 54,56
   54 IF (NWORDS. EQ. 0) GO TO 55 $ M=NLRS+1
      CALL WRITMS (20, WW, VHORDS, M, KREWRIT)
   55 CALL PACK2(N, W, MPT1)
      PRINT 50, INW1, INW2 $ D) 550 I=1, INWL $ M=I+2 $ N=M+INH1
  550 PRINT 51, I, WW(M), WA(N)
      CALL WRITMS (20, WH, NHORDS, 1, KREWRIT)
   56 IF (KQKLOOK) 57,62
   57 DO 61 I=1,4
      ENDFILE I $ BACKSPACE I $ BACKSPACE I
READ(1,58) RECORD
   58 FORMAT (1 3A10, A7)
      IF (IO EOF PE(I)) 59,61,61
   59 PRINT 60,I
   60 FORMAT (*-FILE*12* LAST RECORD*/)
      PRINT 58, RECORD
   61 CONTINUE
   62 RETURN $ END
```

FUNCTION TO EOF PE(J) C.... THIS FUNCTION CHECKS FOR NORMAL, END-JF-FILE, AND PARITY-ERROR C CONDITIONS ON UNIT J FOLLOWING A BINARY READ. DATA KOUNT/0/ KDUNT = KOUNT +1 C NORMAL. K=-1 IF (EOF (J)) 10, 11 C.... END OF FILE. 10 K= U \$ PRINT 20 \$ GO TO 13 11 IF (IOCHEC(J))12,14 C.... PARITY ERROR IN OR AFTER RECORD INDICATED. 12 K=1 \$ PRINT 21 13 PRINT 22, J, KOUNT 14 IO EOF PE=K 20 FORMAT(24H0 ***** END OF FILE *****)
21 FORMAT(25H0 ***** PARITY ERROR *****) 22 FORMAT (* UNIT *12,16X* RECORD *14) RETURN \$ END

E OBSERVE 74/74 OPT=1

21 IF (KTYPE.AND. 8) 22, 230

FTN 4.5+414

SUBROUTINE OBSERVE C.... THIS ROUTINE SELECTS THE TYPES OF DATA REQUESTED FROM THE DATA FILE AND PLACES THEM IN AN INCREASING SEQUENCE IN STORAGE FOR USE BY C PROGRAM ESTHATE. COMMON/SENSORS/SEM4(18), COILS(3,2) COMMON/OBSH/IH, JH, 4(1) COMMON/PARAMS/IQ(33), KDAFA, KTYPES, MAXDAFA, IA, JA, KA, IM, JM, KM, MD C.... THE FOLLOWING COMMON STATEMENT IS DEPENDENT ON THE DATA FILE USED. COMMON/BUFF/LBUFF(+), W(127) DIMENSION DATA(1), [DATA(1) EQUIVALENCE (H(19), ND), (H(20), DATA, IDATA) COMMON/TORQUES/COL.(3),TORQMAG(3),DENCOEF COMMON D(36), T(20), LOC(20), MM(4), LM1(4) DIMENSION LM2(4),LM3(4) DIMENSION COILSP (3, 2) DATA COIL, COILSP/9 . 0 . / DATA KMASK/777777777777777777748/ LH2(3)=LH2(2)=LH2(1)=JH \$ LH3(3)=LH3(2)=LH3(1)=KH LM2(4)=JA \$ LM3(+)=KA RETURN ENTRY OBSERVI C.... SELECT DATA FROM DATA FI.E. KDATA=K=MM(4)=MM(3)=MM(2)=MM(1)=0 KCOUNT=0 LM1(3) = LM1(2) = LM1(1) = IM \$ LM1(4) = IA20 1F(K.EQ.ND) GO TO 31 J=MD*K+1 \$ K=K+1 1=KTYPE=IDATA(J+2) \$ IF (I.GT.2) I=I. AND.KMASK IF (I. AND. KTYPES) 21, 20

C.... STORE COIL DATA. 22 L=KTYPE-7 \$ DO 23 I=1,3 23 COILSP(I,L)=DATA(J+1) + COILS(I,L) CALL MATRIX(21,3,1,0,COILSP,3,COILSP(+),3,COIL,3) \$ GO TO 20 230 IF (KTYPE. AND. 16) 231, 24 C SAVE THE ONE-HALF-RHO-V-SQUARED. 231 DENCOEF=DATA(J+3) \$ GO TO 20 C.... SAVE OTHER TYPES OF DATA FOR PROCESSING. 24 IF (KTYPE.LE.2) GO TO 26 \$ L=MOD(KTYPE,9)-3 MM(L)=MM(L)+1 \$ IF(MM(_).EQ.LM1(L))25,20 25 LM1(L)=LM1(L)+LM3(_) \$ IF(LM1(L). GT. LM2(L)) LM1(L)=0 26 KDATA=KDATA+1 \$ [(KDATA)=DATA(J) \$ LOC(KDATA)=K KCOUNT=KCOUNT+1 \$ IF(K[YPE.EQ.1) KCJUNT=KCOUNT+2 \$ GO TO 20 C.... LIMIT DATA IF NECESSARY. 31 L=KCOUNT-MAXDATA & IF(_.GT.D) KDATA=KJATA-L C.... RETURN WHENEVER NO DATA IS SELECTED OR NO ORDERING OF DATA IS C NEEDED. IF (KDATA-1) 40, 38, 310 C.... ORDER THE DATA IN AN INCREASING SEQUENCE BY TIME. 310 DO 37 I=2, KDATA \$ J=I-L TEST=T(I) \$ IF(TEST.GE,T(J)) GO TO 37 \$ LO=LOC(I) \$ L=I 32 J=J-1 \$ IF(J) 33,34 33 IF (TEST.LT.T(J)) 32,34 34 J=J+1 35 LM1=L-1 \$ T(L)=T(LM1) \$ LOC(L)=LOC(LM1) L=L-1 \$ IF(L, EQ, J) 36,35 36 T(J) = TEST \$ LOC(J) = LO 37 CONTINUE C.... STORE THE SELECTED DATA.

38 DO 39 I=1, KDATA \$ L=MDF (LOC(I)-1)+1 \$ J=MDF (I-1)+1

39 CALL MOVLEY (DATA (L), D(J), ND)

40 RETURN \$ END

SUBROUTINE PACK (N, V, M) C.... THIS ROUTINE STORES DATA BEFORE IT IS OUTPUT AS A SINGLE LOGICAL C RECORD. THE RANGE OF THE DATA IS ALSO COMPUTED. DINENSION V(1), VMIN(50), VMAX(50) COMMON/PACKED/NLRS, NWORDS, VV(5 12) EQUIVALENCE (VV(1), IWD), (VV(2), J) C.... MAXIMUM NUMBER OF AORDS IN A LOGICAL RECORD IS 512. C.... MAXIMUM NUMBER OF ADROS IN A GROUP IS 50. DATA MAXU/512/, MAXAD/50/ C.... INITIALIZE PARAMETERS. NLRS = 0 IWD=N=MING(N, MAXWD) \$ VGP=(MAXD-2)/IWD DO 1 K=1, IND \$ VMIN(K)=1.699 1 VMAX(K)=-1.E39 NWORDS=J=0 KETURN ENTRY PACK1 C.... STORE THE DATA. IF (M. EQ. 1) J=0 IF (J. NE. 0) GO TO 3 \$ M=0 \$ NLRS=NLRS+1 3 J=J+1 \$ N=MINO(N, IHO) \$ L=IHO+(J-1)+2 00 2 K=1,N VI=V(K) \$ IF(VI.LI.VMIV(K)) VMIN(K)=VI IF (VT.GT.VMAX(K)) VMAX(K) = VT 2 VV(L+K)=VT IF (J. EQ. NGP) M=1 NWORDS=L+IWD RETURN ENTRY PACK2 C.... READ OUT THE STORES RANGE VALUES. NWCRDS=2*IWD+2 \$ J=NLRS CALL MCVLEY (VMIN, VV (3), IND) \$ CALL 40 VLEY (VMAX, VV (3+IWO), IWO)

E DIAGNAL 74/74 OPT=1

RETURN \$ END

FTN 4.5+414

SUBROUTINE DIAGNA_(N,X,XX,D,IP,P)

C.... UTILITY SUBROUTINE TO MOVE THE N-DIMENSIONAL STATE VECTOR X INTO
C XX AND TO MAKE THE N-)IMENSIONAL VECTOR) THE DIAGONAL MATRIX P.

C.... NOTE. IP IS COLUMN SIZE OF MATRIX P.

DIMENSION X(1),XX(1),D(1),P(1)

CALL MOVLEV(X,XX,N)

DO 2 I=1,N \$ L=I^P(I-1)

DO 1 K=1,N \$ J=K+L

1 P(J)=0.

J=I+L

2 P(J)=D(I)

RETURN \$ END

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